

Activated Sludge – Evolution to Nitrogen Removal

Maryland Center for Environmental Training

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Activated Sludge – Evolution to Nitrogen Removal

WWW 5880

7 contact hours

9 CC10 hours

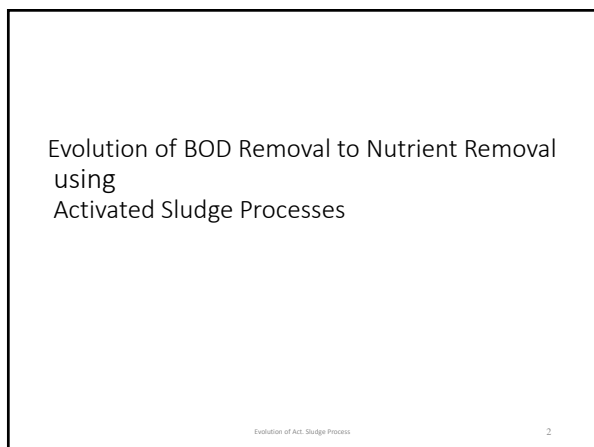
What do you know about the various activated sludge configurations currently used, available, and evolving for activated sludge, BNR, and ENR processes? The objective of this class is to give activated sludge plant operators a more in-depth understanding of the activated sludge process. With this understanding, effluent quality variability and process energy usage can be reduced. Topics to be presented include: wastewater characterization, biological N & P removal, the importance of sludge quality, measuring and controlling sludge quality, WAS flow control, RAS flow optimization, secondary clarifier performance diagnostic testing. Specifically, types of aeration diffusers (mechanical, fine bubble, and membranes) and blowers (positive, multistage, single stage, and high speed) will be addressed. The influence of MCRT and MLSS will also be addressed as to the efficiency, ease (or difficulty) and cost of aeration. Finally, helpful operating hints will be provided based on experiences from operating facilities.

1. Describe the activated sludge process in detail.
2. Identify methods for nitrogen and phosphorus removal
3. Identify how to measure and control activated sludge quality.
4. Describe how to complete secondary clarifier performance diagnostic testing.
5. Discuss the influence of MCRT and MLSS as it relates to efficiency.

Agenda:

- | | |
|---|--------------|
| 1. Introduction | (30 minutes) |
| 2. Activated Sludge Process | (60 minutes) |
| a. Effluent quality variability | |
| b. Process energy | |
| 3. Wastewater Characterization | (90 minutes) |
| 4. Biological N & P Removal | (90 minutes) |
| 5. Sludge Quality | (60 minutes) |
| a. Measuring | |
| b. Controlling sludge quality | |
| 6. WAS flow control and RAS flow optimization | (30 minutes) |
| 7. Secondary clarifier performance diagnostic testing | (30 minutes) |
| a. Aeration diffusers | |
| b. blowers | |
| 8. MCRT and MLSS | (30 minutes) |





Process Training Sessions

Before class starts, please:



- **Sign in** on Attendance Sheet
- **Fill out** Registration Form, if appropriate

During class, please:

- **Asks questions**
- Feel free to get up and leave the classroom at any time (i.e., rest rooms, phone calls, etc.)
- **Answer questions** on post test

After class, please:

- **Fill out** a Class Evaluation
- **Pick up** Attendance Card, if appropriate



Housekeeping

- 1-day class
- Start class – 8:00 am
- 10-minute Breaks – every hour
- Lunch ~ 11:30 am – 12:30 pm
- End class ~ 3:30 to 4:00 pm



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Instructor Expectations

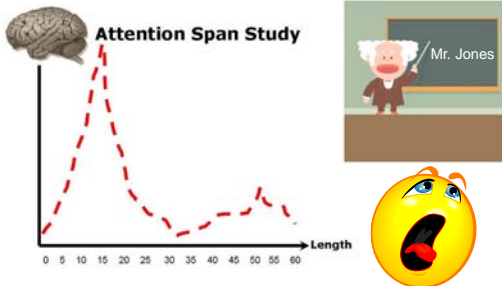
- Begin and end class on time
- Be interactive – participate at your own comfort level
- Share experiences and needs
- Less lecture, more discussions
- Keep it simple
- **Make this an enjoyable and informative experience!**



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Student Attention Span - Lectures



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Discussions

- Student involvement in class discussions is encouraged:
 - To keep students attentive
 - To help students retain information



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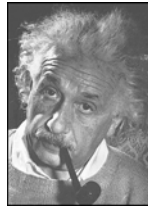
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The Guiding Expectation

“Things should be made as simple as possible -- but no simpler.”

Albert Einstein

www.physik.uni-frankfurt.de/~ir/physpiceinstein.html



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Ground Rules

- Discussion is encouraged; share experiences
- Use terms we all can understand
- Everyone is different, so please show respect for others in the room
- Express opinions - of things, not people
- Maintain confidences



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Ice Breaker

- Before we start, let's introduce ourselves.
 - Name,
 - What do you do, and
 - What are your learning needs?

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Introduction

Objectives, Focus, and Agenda

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Purpose of Today's Class

- Discuss:
 - Activated sludge history and process fundamentals
 - Activated sludge processes for:
 - BOD Removal
 - Nutrient (TN and TP) Removal
 - Instrumentation, Control, and Automation (ICA)

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Purpose of Today's Class

- To discuss the Activated Sludge biological treatment processes
- To discuss Activated Sludge process parameters:
 - Hydraulic and organic loadings
 - F:M/MCRT/SRT
 - Detention times
 - Instrumentation and automation
- To discuss the evolution of Activated Sludge processes
 - from BOD removal to nutrient removal

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Participant Focus

- What information can you use at your work?
 - Aeration and sedimentation fundamentals
 - Activated Sludge troubleshooting
 - Meeting BOD, TSS, nutrient discharge standards
- What information can you contribute to the discussion?
 - Aeration practices
 - Solutions to sludge settling issues

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Class Outline

- Introduction
- Activated Sludge
- Nitrification/Denitrification
- BNR – Biological Nutrient Removal
- ENR – Enhanced Nutrient Removal
- Phosphorus Removal

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Introduction

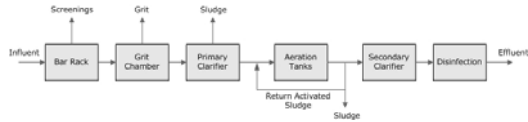
Definitions and Acronyms

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Activated Sludge WWTP

- Wastewater (e.g. municipal wastewater) goes through several stages in which different compounds are removed



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Definitions

- Bar Rack** – where coarse solids are removed, such as sticks, rags, and other debris in untreated wastewater by interception. Use fine screens can remove even floatable matter and algae
- Grit Chamber** – where grit is removed consisting of sand, gravel, cinders, or other heavy solid materials that have settling velocities or specific gravities substantially greater than those of the organic putrescible solids in wastewater

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Definitions

- **Primary Clarifier** – where water has a certain retention time so that the heavy organic solids can settle out (suspended solids). Efficiently designed and operated primary sedimentation tanks should remove from 50 to 70 percent of the suspended solids and 25 to 40 percent of the BOD

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Definitions

- **Aeration Tank** – where the mixed liquor is aerated. By aerating the mixed liquor, the soluble substrate becomes biomass solids
- **Secondary Clarifier** – where biomass solids settle out
- **Disinfection** - where chlorine or UV is used to make effluent free of disease-causing organisms

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Biological Treatment

- **Activated Sludge**
 - MLSS – Mixed Liquor Suspended Solids
 - MLVSS – Mixed Liquor Volatile Suspended Solids
 - WAS – Waste Activated Sludge
 - RAS – Recycled Activated Sludge
- **Activated Sludge Process Control:**
 - DT – Detention Time, Tank volume/flow rate, V/Q, hours
 - MCRT/SRT – Mean Cell/Solids Retention Time, days
 - F:M – Food-to-Mass ratio, BOD/MLVSS
 - SV – Sludge Volume after 30 minutes
 - SVI – Sludge Volume Index, $SV \times 10,000/MLSS$

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Biological Treatment

- BNR/ENR – Biological/Enhanced Nutrient Removal
 - Anaerobic – Soluble BOD uptake and Phosphorus Release
 - Anoxic – Denitrification
 - Aerobic – Nitrification
 - IR or NR– Internal Recycle /Nitrate Recycle

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Acronyms

- BNR – Biological Nutrient Removal
- ENR – Enhanced Nutrient Removal
- TMDL – Total Maximum Daily Loading
- MLE – Modified Ludzack-Ettinger BNR Process
- IFAS – Integrated Fixed Film Activate Sludge
- MBBR – Mixed Bed Bioreactor
- COMAMMOX – COMplete AMMonia OXidation
- ANAMMOX – ANaerobic AMMonia OXidation

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Microorganisms

- **Aerobic** (Oxic) - Organisms requiring, or not destroyed, by the presence of free oxygen
- **Anoxic**: Organisms requiring, or not destroyed, by the absence of free oxygen; nitrates (NO_3) are present.
- **Anaerobic** - Organisms requiring, or not destroyed, by the absence of free oxygen and NO_3
- **Facultative** - Organisms able to function both in the presence or absence of free oxygen
- **Heterotrophic** - Organisms that use organic materials as their source of cell carbon
- **Autotrophic** - Organisms able to use carbon dioxide and other inorganic matter as their source of carbon
- **Filamentous** – Bulking organisms that grow in thread or filamentous form

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Nutrients - Overview

Part of the Periodic Table

13	14	15	16	17
B	C	N	O	F
10.81	12.01	14.01	15.99	19.00
13	14	15	16	17
Al	Si	P	S	Cl
26.98	28.09	30.97	32.07	35.45
31	32	33	34	35
Ga	Ge	As	Se	Br

- ✓ Both Phosphorus and Nitrogen are considered essential for plant and animal life
- ✓ Both are called nutrients

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Introduction

1972 Clean Water Act (CWA)

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Clean Water Act (CWA)

- The 1972 Clean Water Act:
 - Set the basic structure for regulating point source discharges of pollutants into US waterways
 - Gives EPA authority to set **water quality standards** for contaminants:
 - Attain water quality levels that make surface waters safe to fish and/or swim in
 - Restore and maintain the chemical, physical, and biological integrity of the nation's waterways

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Clean Water Act (CWA)

- Water Quality Concerns:
 - BOD (Biological treatment)
 - TSS (Sedimentation and filtration)
 - Coliforms (Disinfection)
- Nutrients:
 - Nitrogen (Nitrification and denitrification)
 - Phosphorus (Biological uptake and chemical precipitation)

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Water Use

- WWTP discharge standards are set to meet water quality standards:
 - In waterways
 - Aquatic and marine life
 - Water contact sports
 - Swimming
 - Boating
 - Fishing
 - For downstream water users:
 - Domestic water supplies
 - Industrial water supplies
 - Agriculture water supplies



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Clean Water Act (CWA)

- EPA can/will impose more stringent **water quality discharge standards** for contaminants:
 - If chemical, physical, and biological integrity of the receiving water requires more removal; e.g., BNR to ENR program in the Chesapeake Bay
 - As new technologies become available to offer cost effective solutions to water quality problems; e.g., automated SBRs for WWTPs < 0.5 MGD

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Clean Water Act (CWA)

- The CWA makes it unlawful for any person to discharge any pollutant from a point source into navigable waters unless a NPDES discharge permit is obtained
- NPDES - National Pollutant Discharge Elimination System
- WWTPs are self-monitored
 - Monthly "Discharge Monitoring Reports" (DMRs)
- EPA has delegated monitoring responsibility to states

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Goals of Wastewater Treatment

- Removal of:
 - **Suspended solids and organic matter** (cBOD and nBOD) to limit pollution
 - **Nutrients** (TP and TN) to limit eutrophication
 - **Microbiological contaminants** to eliminate infectious diseases
- Required levels of treatment are based on NPDES regulations as prescribed in issued discharge permits

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Nutrient Removal "Driver"

Chesapeake Bay Regulations

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Nutrient Removal

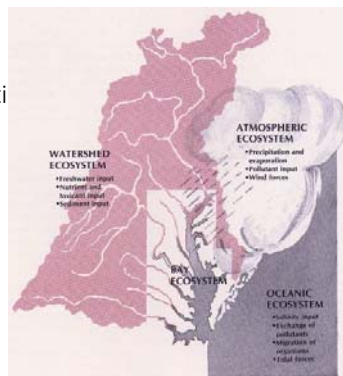
- **Why remove Nutrients (nitrogen and phosphorus):**

- Nutrients contribute to algae growth
- Excess algae growth (Eutrophication) causes water quality issues:
 - Loss of water clarity
 - Limitation on sunlight penetration
 - Oxygen depletion
 - Fish and marine life die-off
 - Submerged aquatic vegetation (SAV) die-off

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Ecosystems Affecting the Bay



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Chesapeake Bay Watershed

- The largest estuary system in the contiguous United States
- Watershed is almost 64,000 square miles
- Surface area of the Bay is 3,830 square miles
 - Of these, 153 square miles are tidal fresh waters
 - 3,562 square miles constitute the mixing zone
 - 115 square miles are salt waters

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The Chesapeake Bay Program

- In 1983, the Chesapeake Bay Program (CBP) created
 - In a 1987 Agreement, water quality targets (40% less than 1985 conditions) for 2000 were established
- Chesapeake Bay 2000 Agreement
 - USEPA, MD, VA, DC, PA and the Chesapeake Bay Commission – Signatories to agreement
 - USEPA has the lead on setting water quality standards for the Bay
 - States develop plans (Tributary Strategies) and implement actions
 - 2010 - Target Date to meet water quality standards, remove the Bay from the impaired waters list, and to avert the need for TMDLs
- Beyond 2010 – TMDLs and consent decrees
 - 2017 is new interim target date
 - 2025 is new target date



BNR Program

- EPA created the Chesapeake Bay Program in 1983; first Chesapeake Bay agreements signed in 1987
- BNR Programs initiated by Bay states
- For WWTPs greater than 0.5 mgd:
 - 95% of wastewater discharged into the Bay
 - Grant funding available for WWTP upgrades
- WWTP discharge goals:
 - Reduce TP from ~ 6 mg/l to < 3.0 mg/l
 - Reduce TN from ~ 20 mg/l to < 8.0 mg/l

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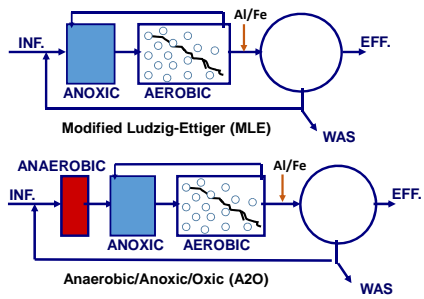
BNR Program

- To reduce total phosphorus concentrations, most WWTPs began add chemicals like FeCl_3 or alum
- To reduce total nitrogen concentrations, most WWTPs initiated a capital improvement project to add "Pre" anoxic zones to already existing nitrification processes for partial denitrification

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Biological Nutrient Removal



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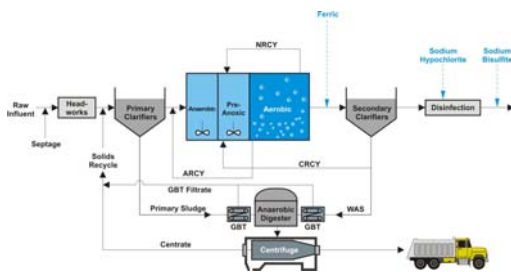
BNR



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Typical BNR Activated Sludge System



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ENR Program

- New Chesapeake Bay Agreement enacted in 2000; ENR Program began in that same year
- For WWTPs greater than 0.5 mgd
 - 95% of wastewater discharged into the Chesapeake Bay
 - Grant funding available for upgrades
- WWTP discharge reduction goals:
 - Reduce TP from $< 3.0 \text{ mg/l}$ to $< 0.3 \text{ mg/l}$
 - Reduce TN from $< 8.0 \text{ mg/l}$ to $< 3.0 \text{ mg/l}$

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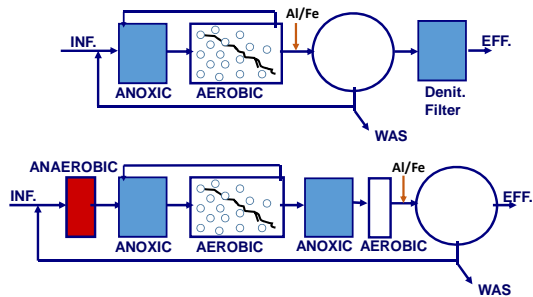
ENR Program

- To further reduce total phosphorus concentrations, most WWTPs began adding increased quantities of chemicals
- To further reduce total nitrogen concentrations, most WWTPs initiated a capital improvement project to add "Post" anoxic zones to already existing BNR facilities

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Enhanced Nutrient Removal



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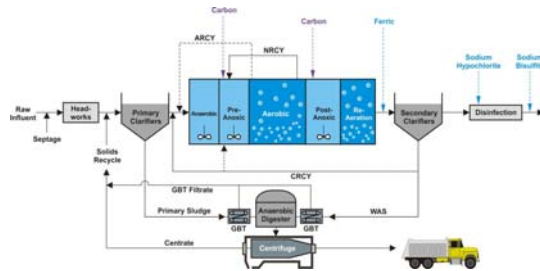
ENR



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Typical ENR Activated Sludge System



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Enhanced Nutrient Removal (ENR)

- Over the past two decades, BNR facilities have been upgraded with automation and new technologies to improve nitrogen removal efficiencies:

- Integrated Fixed Film Activated Sludge (IFAS) to enhance nitrification
- Mixed Bed Bio-reactors (MBBR)
- Biological Aeration Filters (BAF) for nitrification
- Tertiary denitrification filters

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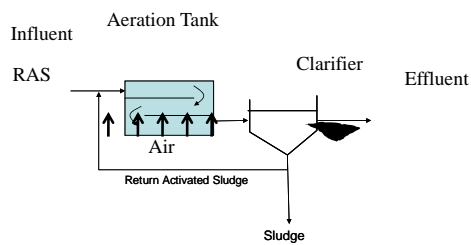
Activated Sludge Process

Process Overview

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Typical Activated Sludge Process



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Basic Process Components

- Aeration Tank (Reactor)
 - Mixed liquor
 - Mixed liquor suspended solids (MLSS) - Biomass
 - Aeration (and mixing) system
- Secondary clarifier
 - Return activated sludge (RAS)
 - Waste activated sludge (WAS)

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Activated Sludge Processes

Activated sludge processes can remove:

1. **cBOD:**
 - Dissolved organic materials
2. **nBOD - Convert ($\text{NH}_3\text{-N}$) to ($\text{NO}_3\text{-N}$)**
3. **Nutrients**
 - Phosphorus
 - Nitrogen
4. **Total suspended solids (TSS):**
 - Suspended organic and inorganic particulate solids

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Process Combinations

- BOD removal (carbonaceous BOD)
- BOD removal and nitrification
- BOD removal and TN removal
 - Nitrification
 - Denitrification
- BOD removal, TN removal, and excess uptake of TP (e.g., Bio-P)

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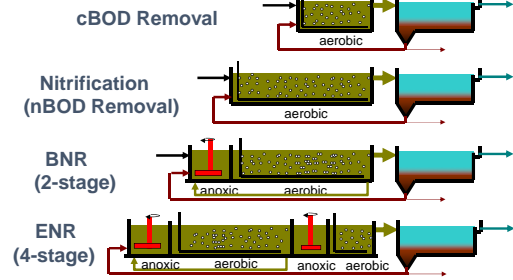
Brief Historical Overview

- 1912 – Aeration of MLSS experiments (US and England)
- 1915 – 1960s:
 - cBOD Removal
 - 30:20 ($\text{BOD}_5\text{:TSS}$) + nitrification - England
 - 30:30 ($\text{BOD}_5\text{:TSS}$) - US
 - Nitrification
- 1960s - 1970s – Phosphorus removal w/chemicals
- 1970s to 2000 – BNR development and application
- Past 30 years – BNR to ENR; filtration; automation

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Evolution of Activated Sludge



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Wastewater Constituent Removal

- **TSS and cBOD Removal** in primary clarifiers and secondary bioreactors/clarifiers
- **TP removal** in primary, secondary, and tertiary
 - Particulate removal
 - Biological uptake
 - Chemical precipitation
- **Nitrification:** Ammonia-N conversion to nitrate-N
- **Denitrification:** Nitrate-N conversion to nitrogen gas

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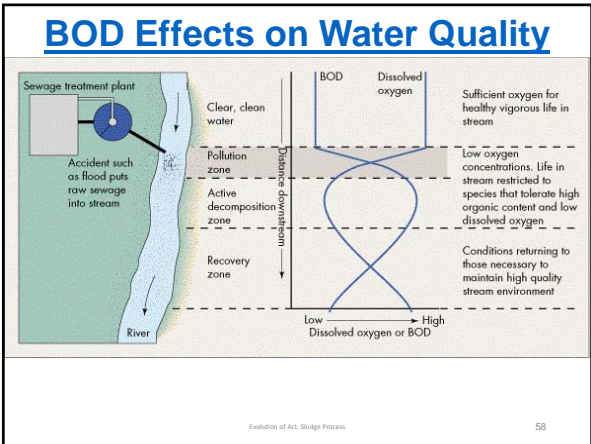
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Key Wastewater Constituents

- **BOD – Biochemical Oxygen Demand**
 - Typically, a five-day test is used to determine the quantity of oxygen used by microorganisms.
 - The higher the BOD concentration, the greater the wastewater strength (organic matter or food).
 - Raw sewage concentrations - 150 to 300 mg/l
 - Valid five-day BOD testing conditions:
 - BOD incubator temperature - 20°C
 - DO uptake - 2.0 mg/l
 - DO remaining after five days - 1.0 mg/l

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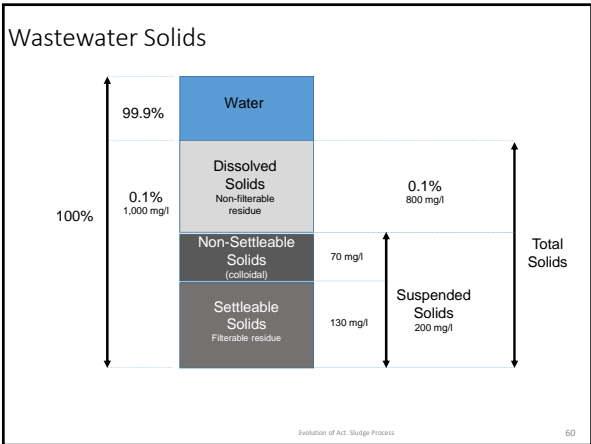
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Key Wastewater Constituents

- TSS – Total Suspended Solids
 - Substances in wastewater that can be removed by physical means
 - Sedimentation and filtration unit processes are used to remove TSS from wastewater
 - Raw sewage concentrations - 150 to 300 mg/l
 - Valid TSS testing conditions:
 - Temperature in a drying oven - 103°C
 - VSS burn off at 550°C

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Key Wastewater Constituents

- pH
 - An expression of the intensity of basic or acidic conditions, 0 (most acidic) to 14 (most basic); 7 neutral
 - Microorganisms most active 6.5 - 8.0
 - Nitrification is inhibited at pH 6.0 or less
- Alkalinity
 - Measure of wastewater ability to buffer pH change
 - Nitrification is inhibited when alkalinity < ~ 60 mg/L
- Pathogenic organisms
 - E-coli indicator
 - Numbers are limited in permit

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Key Wastewater Constituents

- Nutrients
 - TP – Total Phosphorus
 - TN – Total Nitrogen
- Phosphorus and Nitrogen compounds are nutrients that can stimulate production of excess algae in receiving waters
- Typical raw wastewater concentrations:
 - TP – 3 to 6 mg/l
 - TN – 30 to 45 mg/l

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Nutrients

- TN – Total Nitrogen
 - Soluble and particulate
 - Organic nitrogen - N_{org}
 - NH_3 – Ammonia
 - NO_2 – Nitrite
 - NO_3 – Nitrate
- TP – Total Phosphorus
 - Soluble and particulate
 - PO_4 – Ortho-phosphorus
 - Organic
 - Polyphosphates

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Nutrients

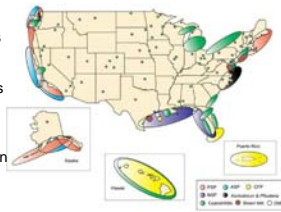
- TN – Total Nitrogen ($N_{org} + NH_3 + NO_3 + NO_2$)
- TP – Total Phosphorus ($PO_4 + P_{org} + P_{poly}$)

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Extent of N and P Impacts

- 14,000 Nutrient-related Impairment Listings in 49 States
- ~80% of Assessed Continental U.S. Coastal Waters exhibit eutrophication
- ~50% of streams have medium to high levels of nitrogen and phosphorus



Occurrence of Algae throughout the U.S.

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Nutrient Removal

Nutrient

•Nitrogen

•Phosphorus

Removal Process

- Nitrification
 - Ammonia Conversion
 - NH_3-N to NO_3-N
 - Oxygen and alkalinity needed
- Denitrification
 - Nitrate Removal
 - NO_3-N to Nitrogen gas (N_2)
 - Carbon source needed
- Physical Incorporation
- Biological Uptake
 - Conventional
 - Excess
- Chemical Precipitation

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Nutrient Removal

FORM	Removal Mechanism	LOT ¹ , mg/L
TN		< 1.5
NH ₃ -N	Nitrification	< 0.1
NO ₃ -N	Denitrification	< 0.1
Org-N:		
Particulate	Solids Separation	< 0.5
Soluble	Ammonification	0.5 – 1.0
TP		< 0.05
Particulate	Solids Separation	< 0.05
Soluble	Biological uptake and chemical precipitation	< 0.05

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Nutrient Discharge Limits - TN

Typical **Total Nitrogen** Standards, mg/l

- Moderate 3.0 – 5.0 (BNR): > 1983
- Bay Target **< 3.0 (ENR): > 2000**
- Severe < 2.5
- Very Severe < 1.5
- LOT/SOA(a) < 1.0

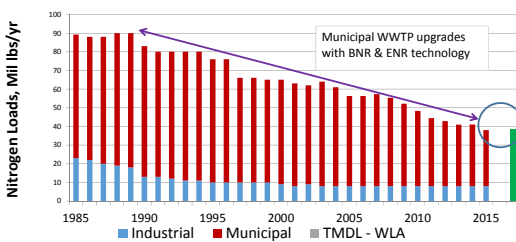
(a) Limit of Technology/State of the Art

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TN Loadings to the Chesapeake Bay Wastewater

(Million pounds/year)



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Nutrient Discharge Limits - TP

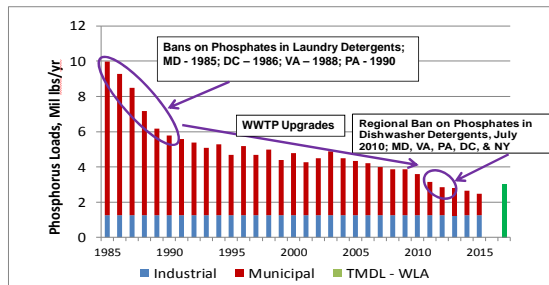
Typical **Total Phosphorus** Standards, mg/l

- Moderate 1.0 - 2.5 (BNR); > 1983
 - Bay Target < 0.3 (ENR); > 2000
 - Potomac River < 0.18 (ENR)
 - Very Severe < 0.1
 - LOT/SOA(a) < 0.05
- (a) Limit of Technology/State of the Art

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TP Loadings to the Chesapeake Bay Wastewater



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IC&A Drivers

- Instrumentation, control, and automation (IC&A)
 - Initiated in the 1970s
 - Major push in the 1980s
 - Meet nutrient regulatory requirements
- Improve process performance – BNR/ENR processes require effective DO control (enough but not too much, or none at all)

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Nitrification-Related Process Instruments and Parameters

- Temperature
- Flow meters
- Flow rates:
 - Effluent
 - WAS
- Solids ret. time (SRT)
- pH/alkalinity
- Airflow distribution
- DO probe(s)
- DO conc., mg/L
- Ammonia probe(s)
- Ammonia conc., mg/L
- Nitrate probe(s)
- Nitrate conc., mg/L

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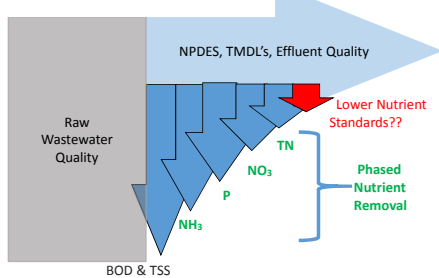
Denitrification-Related Process Instruments and Parameters

- Temperature
- Flow meters
- Flow rates
 - Inflows
 - Internal Recycle
- pH/alkalinity
- DO probe(s)
- DO conc., mg/L
- Nitrate probe(s)
- Nitrate conc., mg/L

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Role and Impact of Nutrients



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How will future regulations affect Activated Sludge Processes?

Regulatory Challenges:

- Clean Water Act (CWA)
- Chesapeake Bay Program
- State Ordinances
 - Nutrients
 - Sludge
- Local Ordinances



October 2018

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Activated Sludge Process

Early History

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Need for Wastewater Treatment



- Epidemics (e.g., cholera) triggered interest in constructing sewage collection systems in large European cities:

- Berlin: 1830
- London: 1830
- Hamburg: 1842

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Open Sewers – 1800s



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Sewage “Farm” – Berlin 1900

- Early wastewater treatment systems were irrigation fields
- Problems with odors



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History: Pre-Activated Sludge

- 1690 – Sewers (Paris, France)
- 1860 – Septic Tank (Louis Moureas)
- 1868 – Trickling Sand Filter Process (Edward Frankland)
- 1882 – Aeration of sewage (Argus Smith)
- 1911 – Chlorination (London, England)
- **1914 – Activated Sludge Process (Arden and Lockett)**

Evolution of Act. Sludge Process

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Early History of Activated Sludge

- 1898 - formation of the Royal Commission on Sewage Disposal in England
- In the early 1900's, England along with most of Europe and the US were seeking small footprint wastewater treatment solutions
- 1912 - Famous "30:20 + full nitrification" effluent standard was adopted in England
- New stringent BOD₅ effluent standard inspired creation of the activated sludge process

Evolution of Act. Sludge Process

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Early History of Activated Sludge

- In 1912, in the US, Clark and Gage at the Lawrence Experimental Station began looking at aerating suspended solids in wastewater
- Lawrence Experimental Station became known as "the Mecca of sewage purification"



Evolution of Act. Sludge Process

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Activated Sludge

- Growth and retention of suspended biological solids using oxygen to remove:
 - Soluble Organics (CBOD, COD)
 - Organic Solids (TSS, VSS)
 - Nutrients
 - Nitrogen
 - Phosphorus



Evolution of Act. Sludge Process

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Early History of Activated Sludge

- In 1912, Dr. Gilbert Fowler from the University of Manchester (England);
 - Began his activated sludge studies in Europe
 - Traveled to the Lawrence Experimental Station (LES) in Massachusetts, (USA)

Evolution of Act. Sludge Process

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Early History of Activated Sludge

- From 1913 – 1915, in England;
 - Lab-scale suspended biomass experiments were performed in England by Edward Ardern and his co-worker, William Lockett under the direction of Dr. Gilbert Fowler
 - In separate studies, Walter Jones of Jones and Attwood, Ltd. developed practical applications of the activated sludge process

Evolution of Act. Sludge Process

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Early History of Activated Sludge

- 1914/1915 - Ardern and Lockett published their research findings on aeration of suspended solids (e.g., MLSS)
 - Added the concept of recycling sludge
 - First to use the term “activated sludge”
- 1915 First full-scale activated sludge plant in Salford, England
 - 80,000 gpd at fill-and-draw operation (SBR)
 - 12,000 gpd at continuous-flow operation (Plug-flow)

Evolution of Act. Sludge Process

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Early History of Activated Sludge

- 1913 English patents by Jones and Attwood, Ltd
 - 25 cents/capita royalties paid by most WWTPs
- 1915 American patent by Leslie Frank (US Public Health officer)

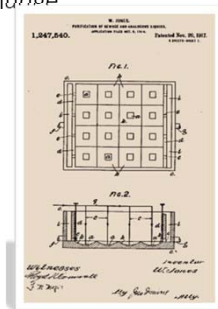


Evolution of Act. Sludge Process

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Early History of Activated Sludge

- Walter Jones' U.S. activated sludge patent 1,947,540 was issued in 1917 and expired in 1934
- The last of the Jones' US patents expired in 1935



Evolution of Act. Sludge Process

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Early History of Activated Sludge

- 1915-1921 Ten full-scale plants in UK
- 1916-1927 Nine full scale plants in US
 - San Marcos, TX (1916)
 - Cleveland, OH (1916)
 - Houston (north), TX (1917)
 - Houston (south), TX (1918)
 - Des Plaines, IL (1922)
 - Calumet, In (1922)
 - Milwaukee, WI (1925)
 - Chicago IL and Indianapolis, IN (1927)

Evolution of Act. Sludge Process

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Early History of Activated Sludge

- Late 1920s – Patent infringement suits were filed by Activated Sludge, Ltd. (ASL), the licensed patentee for Jones and Attwood, Ltd. against US cities of Chicago, Milwaukee, Cleveland, and Indianapolis
- Lawsuits and threats of litigation led to:
 - Shutdown of several activated sludge plants in the US
 - Delays in designing activated sludge processes until ASL patents expired (e.g., 1935)/lawsuits exhausted (e.g., late 1940s)
- Both Chicago and Milwaukee paid large settlements (~\$1.0 million each) to ASL in the 1940s

Evolution of Act. Sludge Process

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Early History of Activated Sludge

- Until 1995, U.S. patents were issued for a term of seventeen years, beginning on the issuance date
- Today, a patent's term still begins on the issuance date, but normally expires twenty years from filing date

Evolution of Act. Sludge Process

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Early History of Activated Sludge

- Most activated sludge development in the US was delayed until the 1950s due to:
 - Process royalties
 - Patent legalities
 - WWII
 - Example: Blue Plains – 1959

Evolution of Act. Sludge Process

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Activated Sludge

Process Description

Evolution of Act. Sludge Process

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Wastewater Treatment

• Secondary (Biological) Treatment

- Purpose - BOD removal
Nitrification
- Processes
 - **Activated sludge (suspended growth)**
 - Fixed film (attached growth)
 - Stabilization Ponds
- Disposal of sludge and scum



Evolution of Act. Sludge Process

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Biological (Secondary) Treatment

- Influent contains high levels of organic material
 - Biological Oxygen Demand – (~150 mg/l)
 - Organic nitrogen – (~20 mg/l)
 - Organic phosphorus – (~2 mg/l)
- Three common biological treatment processes:
 - **Activated sludge**
 - Trickling filters
 - Stabilization ponds (Lagoons)

Evolution of Act. Sludge Process

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Activated Sludge

- **Secondary treatment** - the biological treatment of wastewater:
 - Activated sludge is a type of secondary treatment
 - Removes a high level of biodegradable organic pollutants (BOD) to protect receiving water quality that sedimentation (Primary) alone can't provide
- **Activated Sludge** - a mixture of bacteria, fungi, protozoa (single cell), and metazoan (multi-cell) microorganisms maintained in suspension by aeration or mixing

Evolution of Act. Sludge Process

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Activated Sludge



Evolution of Act. Sludge Process

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Activated Sludge Process

- Aeration and sedimentation tanks
- Oxygen – Air or pure oxygen
- Biomass – MLSS
- TSS, BOD, and TP Removal
- Nitrogen (BNR/ENR) removal
 - Nitrification (Oxic zones)
 - Denitrification (Anoxic zones)
- Need to waste solids to maintain target MCRT and F:M ratios
- Occasional foaming and bulking problems
- May need to add alkalinity in nitrification process

Evolution of Act. Sludge Process

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Activated Sludge Process Tanks

- **Aeration tank** – Tank where air (or oxygen) is injected in the mixed liquor.
- **Clarifier** – "Final clarifier" or "secondary settling tank" where biological floc (the sludge blanket) settles, separating biological sludge from treated water.

Evolution of Act. Sludge Process

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Activated Sludge Process



Evolution of Act. Sludge Process

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Activated Sludge Components

1. Mixing return sludge with wastewater forming a mixed liquor
2. Aeration and agitation of the mixed liquor (biomass - MLSS) for a period of time
3. Separation of activated sludge from the mixed liquor in a sedimentation process
4. Return of the proper amount of activated sludge for mixture with wastewater
5. Wasting of excess activated sludge

Evolution of Act. Sludge Process

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Return Activated Sludge

- The settled activated sludge (biomass) that is collected in a secondary clarifier and returned to the secondary aeration process to mix with incoming wastewater
- The RAS pumps a concentrated population of microorganisms back into the aeration basin
- Centrifugal pumps are commonly used in the RAS line

Evolution of Act. Sludge Process

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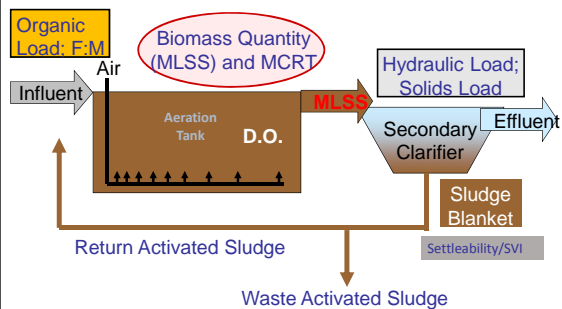
Waste Activated Sludge

- The activated sludge (excess biomass or cell mass) removed from the secondary treatment process.
- For most treatment plants, this will be a portion of the Return Activated Sludge (RAS) flow stream.
- Typical wasting rates: 0.5 to 0.75 lbs/lb BODr

Evolution of Act. Sludge Process

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Operating Parameters



Evolution of Act. Sludge Process

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Activated Sludge

- Oxidizes carbonaceous matter (BOD)
- Nitrifies $\text{NH}_3\text{-N}$ to $\text{NO}_3\text{-N}$
- MCRT/SRT:
 - > 1 day for BOD removal
 - > 7 days for nitrification (Temperature dependent)
- DO concentrations:
 - > 1.0 for BOD removal (Range: 1 – 2 mg/l)
 - > 2.0 for nitrification (Range: 2 – 4 mg/l)
- MLSS concentrations – 2000 to 8000 mg/l
- RAS – 50% of influent flow

Evolution of Act. Sludge Process

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Activated Sludge Environmental Factors

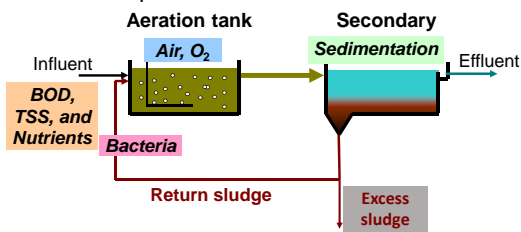
Parameter	Range
Food	Proper amount of food to microorganisms (F:M)
Hydraulic Flow Rate	Within plant design capacity. Excessive flows can result in suspended solids washout
Oxygen	Many of the bacteria in wastewater require between 1 mg/L to 3 mg/L of dissolved oxygen
Temperature	Most microorganisms in wastewater grow best between 10 and 25 degrees C. At >35 to 40 degrees C, thermophilic bacteria will take over
Nutrients	Conventionally a CBOD: Nitrogen: Phosphorus ratio of 100:5:1 is recommended in addition to proper micronutrients such as iron and other trace minerals
pH	Between 6.5-8.5 is recommended
Alkalinity	There needs to be enough buffering capacity to maintain pH. Typically 60 mg/L or more of alkalinity at the end of treatment is desired

Evolution of Act. Sludge Process

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Activated Sludge Process

- Today, the most widely used wastewater treatment process in the USA



Evolution of Act. Sludge Process

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Operating Parameters

- MLSS/MLVSS, mg/l
- Dissolved oxygen, mg/l
- pH and alkalinity
- BOD, TSS, TN, and TP
- Aeration detention time, hours
- Organic loading, lbs BOD/1000 ft³ of aeration tank
- Food/Mass ratio (F/M), lbs BOD/lbs MLSS or MLVSS
- Mean Cell Residence Time (MCRT), days
- WAS rate, Q_w
- RAS, % Q_{in}

Analytical data

Flow data

Evolution of Act. Sludge Process

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Common Formulas for Activated Sludge

Organic Loading Rate: mg/L BOD (or COD) x flow, as MGD (millions of gallons per day) x 8.34

F/M Ratio: Lbs BOD per day/ lbs MLVSS (mixed liquor volatile suspended solids)

Retention time (hours): tank volume (MG) x 24 hours/ flow (MGD)

Solids Residence Time, SRT (days): lbs MLSS in system inventory/ lbs of suspended solids leaving the plant per day via wasting and as suspended solids in the effluent.

Removal percentage: This can be used to determine treatment rates for various parameters: lbs removed/ lbs in influent x 100

Evolution of Act. Sludge Process

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Loading Rates

- Organic loading rate – lbs BOD per day
 - Activated sludge - lbs BOD/day/1000 ft³ of aeration tank
 - < 40 lbs BOD/day/1000 ft³
 - Typical range: 15 to 25 lbs BOD/day/1000 ft³
- Hydraulic loading rate – gpd/ft²
 - Activated sludge clarifiers
 - Range: 300 to 1200 gpd/ft²
- Solids loading rate – lbs TSS per day/ft²
 - Activated sludge clarifiers
 - Range: 12 to 30 lbs TSS/day/ft²

Evolution of Act. Sludge Process

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Organic Loading

- Organic loading is the amount of biodegradable material that exerts an oxygen demand on the biological treatment process.
- The organic strength of the wastewater is usually measured as biochemical oxygen demand (BOD) in milligrams per liter (mg/L).

Evolution of Act. Sludge Process

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Organic Volumetric Loading Rate

- Pounds BOD/day per 1,000 ft³ of aeration tank

$$\text{Lbs/day/1,000 ft}^3 = \frac{Q_{in} \times \text{BOD}_{in}, \text{mg/l} \times 8.34}{V_t}$$

where: Q_{in} = influent wastewater flow, MGD

BOD_{in} = influent BOD concentration, mg/l

V_t = aeration tank volume, 1,000 ft³

Evolution of Act. Sludge Process

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Food-to-Microorganism Ratio

- Food to microorganism ratio (F:M or F/M) is the amount of food (BOD_5) provided to the microorganisms (MLVSS) in the aeration basins
- F:M is determined by dividing the pounds of influent BOD_5 by the pounds of mixed liquor volatile suspended solids (MLVSS) in the aeration tank

Evolution of Act. Sludge Process

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Flow and Hydraulic Retention Time

- The **hydraulic retention time (HRT)** is a measure of the average length of time wastewater remains in a tank, or time for wastewater **flow** to fill up a tank, or to completely replace the contents of a tank
- $HRT = V_t / (Q_{in} / (24 \text{ hrs/day}))$, hours
Where: V_t is in MG
 Q_{in} is in MGD
- Typically, flow is in MGD, so flow must be converted to MG per hour:
e.g., MGD/(24 hours/day)

Evolution of Act. Sludge Process

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SRT or MCRT

SRT - Solids Residence Time (**Reactor only**)

Pounds of **MLSS in aeration tanks**
Pounds TSS wasted + Pounds TSS lost in eff.

MCRT - Mean Cell Resident Time (**Reactor and Clarifier**)

Pounds of **MLSS in aeration and clarifier tanks**
Pounds TSS wasted + Pounds TSS lost in eff.

$MLSS, \text{mg/l} \times (\text{aeration} + \text{clarifier Vols.}) \times 8.34$
Pounds TSS wasted + Pounds TSS lost in eff.

Evolution of Act. Sludge Process

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MCRT

- Mean cell residence time (MCRT) equals the pounds of solids in the system (in the aeration tank and secondary clarifier) divided by the pounds of solids leaving the system (pounds of waste activated sludge plus pounds of clarifier effluent solids).
- Mean Cell Residence Times:
 - BOD removal, w/o nitrification - 1 to 3 days
 - BOD removal and nitrification - 8 to 12 days

Evolution of Act. Sludge Process

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SRT/MCRT Calculations



The average length of time, in days that an organism remains in the secondary treatment system

$\frac{\text{Biomass in System, pounds}}{\text{System per day}}$ Pounds of solids leaving

$\frac{\text{Biomass in System, pounds}}{\text{Pounds TSS wasted} + \text{Pounds TSS lost in eff.}}$

Evolution of Act. Sludge Process

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Process Control

- Three physical properties are monitored in wastewater:
 - Liquid flow: Wastewater, sludge quantities, chemical addition
 - Concentrations: MLSS, nutrients, sludge solids
 - Gases: air, digester gas

Evolution of Act. Sludge Process

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Common Controlled Variables

- Aeration
 - Set DO levels in different sections of process basin
 - Control aeration in time (cyclic aeration)
- Chemical Addition
 - Methanol, Ferric/Alum, Hypochlorite feed rates

Evolution of Act. Sludge Process

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Common Controlled Variables

- Internal Recycles
 - Set flow rates based on process conditions
- Sludge Wasting Rate
 - Control Solids Retention Time – One of the most important parameters for advanced BNR
- Others?
 - Creative thinking is key to advancement!

Evolution of Act. Sludge Process

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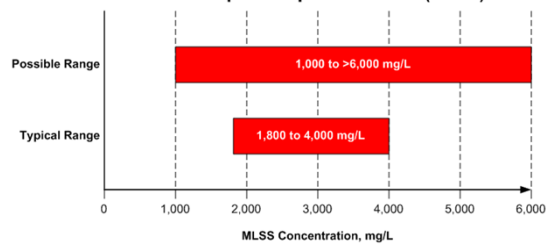
Activated Sludge Processes

Observations – Aeration Tank

Evolution of Act. Sludge Process

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Mixed Liquor Suspended Solids (MLSS)



thewastewaterblog.com

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Aeration Tank Observations

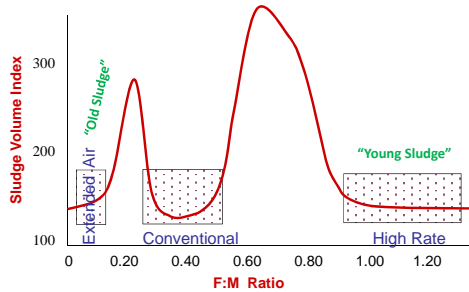
- Foam:
 - Low MCRT – off white, small amounts
 - High MCRT – dark brown, larger amounts
- Color of mixed liquor:
 - Low MCRT - chocolate brown
 - High MCRT – dark chocolate brown



Evolution of Act. Sludge Process

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Process Variations and F/M Ratio



Evolution of Act. Sludge Process

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Young Sludge

- Start-up or High BOD Load
- Few Established Cells
- Log Growth
- High F:M
- Low MCRT



Evolution of Act. Sludge Process

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Young Sludge



Poor Flocculation
Poor Settleability
Turbid Effluent

White
Billowing
Foam

High O₂
Uptake Rate



Evolution of Act. Sludge Process

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Old Sludge

- Slow Metabolism
- Decreased Food Intake
- Low Cell Production
- Oxidation of Stored Food
- Endogenous Respiration
- Low F:M
- High CRT
- High MLSS



Evolution of Act. Sludge Process

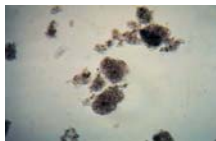
128

Old Sludge

Dense, Compact Floc

Fast Settling

Straggler Floc



Evolution of Act. Sludge Process

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Spray Wash for Foam Control



Evolution of Act. Sludge Process

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Activated Sludge Process

Aeration

Evolution of Act. Sludge Process

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Let's Focus on Oxygen



Evolution of Act. Sludge Process

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Aeration



Evolution of Act. Sludge Process

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Aeration

- Purpose of aeration:
 - To dissolve oxygen into wastewater so that activated sludge microorganisms can utilize it to break down organic material
- Aeration is also used for mixing purposes and to enhance biological growth

Evolution of Act. Sludge Process

134

Aeration

- Conventional activated sludge is an aerobic process. Many organisms in the activated sludge process need free oxygen (O_2) to convert food into energy for their growth.
- Typical Dissolved Oxygen (DO) concentrations:
 - Less than 1 mg/l - bulking potential
 - BOD removal - normal 1 to 2 mg/L
 - "Nitrification" - 2 to 4 mg/l

Evolution of Act. Sludge Process

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Aeration

- BOD Removal
- Nitrification – convert NH_3 to NO_3

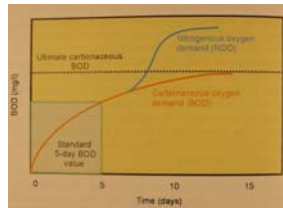


Evolution of Act. Sludge Process

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Oxygen Requirements

- Biological treatment:
 - **cBOD removal** – from organic matter and suspended solids
 - **nBOD removal** – Nitrification, convert ammonia nitrogen to nitrate nitrogen (before denitrification)



Evolution of Act. Sludge Process

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Air Demand Requirements, lbs/day

Treatment	Equation	lb O ₂ /lb oxidized
Organic Removal	$\text{BOD}_{\text{oxidized}} = \text{BOD}_{\text{inf}} - \text{BOD}_{\text{eff}}$	1.0 – 1.2
Nitrification	$\text{TKN}_{\text{oxidizable}} = \text{TKN}_{\text{inf}} - \text{TKN}_{\text{assimilated}}$	4.6
	$\text{TKN}_{\text{oxidized}} = \text{TKN}_{\text{oxidizable}} - \text{TKN}_{\text{eff}}$	

NPDES Effluent Requirement	OTR Equation
BOD ₅ Limit	$1.2 * \text{BOD}_{\text{oxidized}}$
BOD ₅ + NH ₃ -N Limit	$1.2 * \text{BOD}_{\text{oxidized}} + 4.6 * \text{TKN}_{\text{oxidized}}$

Evolution of Act. Sludge Process

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Aerobic Processes

- Aerobic processes require O_2 for removal of organics (BOD) and conversion of ammonia-N to Nitrate-N (nitrification)
- Oxygen can be supplied by air or pure O_2
- Oxygen can be delivered through mechanical (surface) or diffused aerators
- Aeration in activated sludge processes serve two purposes:
 - To satisfy oxygen needs
 - Mixing

Evolution of Act. Sludge Process

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Mixing requirements

- Generally for air Activated Sludge systems, satisfying oxygen demand supplies enough mixing to keep biomass in suspension
- Mixing may be limiting for pure O_2 and extended aeration systems
- In these cases additional mixing (power) must be supplied

Evolution of Act. Sludge Process

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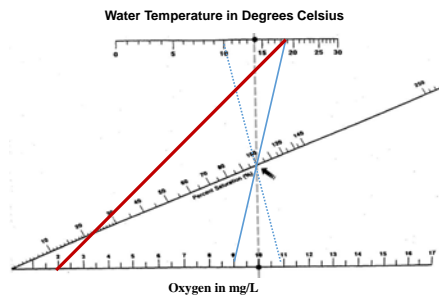
Importance of Dissolved Oxygen

- Oxygen is sparingly soluble in water
- DO is a growth-limiting substrate
- Critical oxygen concentration is about 10% to 50% of DO saturation in water
 - 10% minimum saturation (~ 1.0 mg/l DO) for BOD removal to less than 15 mg/L
 - 20% minimum saturation (~ 2.0 mg/l DO) for complete nitrification

Evolution of Act. Sludge Process

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D.O. - Percent Saturation in Water

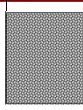
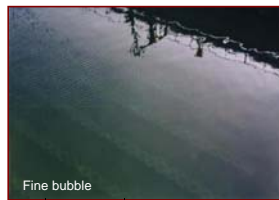


Source: Department of Fisheries and Aquatic Sciences, University of Florida

Evolution of Act. Sludge Process

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Gas transfer devices



Evolution of Act. Sludge Process

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Mechanical Aerators

Two basic types commonly used
Low speed surface aerators
Submerged turbine aerators

Low speed surface aerators

- Most common type in AS
- O_2 transfer rate low
- Dissipate heat quickly

Submerged turbine aerators

- Higher gas transfer efficiencies
- High energy requirements



Evolution of Act. Sludge Process

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Types of Air Blowers

- Multistage Centrifugal
- Positive Displacement
- Single Stage Centrifugal (integral gear)
- High Speed Direct Drive (turbo)



Evolution of Act. Sludge Process

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Coarse Bubble

- Application
 - Nearly every process and wastewater
 - Industrial applications - zero maintenance
 - Stainless steel construction
 - 30 year design life
- Efficiency
 - Spiral roll
 - 0.7-0.9% SOTE per ft submergence
 - 3-4 lb oxygen/kwh
 - 60% greater power than fine bubble fixed
- Maintenance
 - Near zero maintenance
 - Required maintenance - hardware, grit, diffusers
 - Inspection every 3-5 years



Evolution of Act. Sludge Process

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Fine Bubble

- Application
 - Nearly every process and wastewater
 - Media sensitivity
 - Low oil membrane disc
 - Membrane 8-10 year minimum life
 - Ceramic 10-20 year life w/ PM
- Efficiency
 - Most efficient device
 - Greater than 2-3% SOTE per ft submergence
 - 8-10 lb oxygen/kwh
- Maintenance
 - Required maintenance - hardware, grit, leaks, diffusers
 - Ceramic annual cleaning
 - Membrane cleaning every 2 - 3 years



Evolution of Act. Sludge Process

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Activated Sludge

Microbiology

Evolution of Act. Sludge Process

1

Mixed Liquor Suspended Solids

- The concentration of suspended solids in an aeration tank is expressed in mg/L.
- MLSS consists mostly of microorganisms and non-biodegradable suspended matter.
- The volatile portion is used as a measure of microorganisms present in the aeration tank.

Evolution of Act. Sludge Process

2

Microbial Ecology of Activated Sludge

- Biological processes removing carbonaceous BOD under aerobic conditions employ chemo-heterotrophic bacteria for oxidation of organics
- Approximately 95% of biomass in activated sludge processes is chemo-heterotrophic bacteria

Evolution of Act. Sludge Process

3

Microbial ecology of aerobic processes

- Remaining 5% of biomass consists of protozoans and metazoans
 - Presence of protozoans and metazoans indicates toxic free (e.g., NH_3) environment
 - Ciliated protozoan indicate good settling sludge
 - Free swimming protozoan indicates dispersed growth (poor settling)
 - A small fraction of biomass is multi-cellular metazoans



Evolution of Act. Sludge Process

4

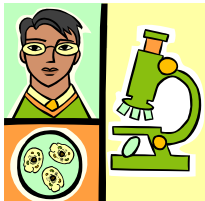
Activated Sludge

- Protozoa (single-cell organisms)
 - Amoeba
 - Flagellates
 - Free-swimming ciliates
 - Stalked ciliates
- Metazoans (multi-cell organisms)
 - Rotifers
 - Nematodes
 - Worms
 - “Water Bears”

Evolution of Act. Sludge Process

5

Microscope Exam

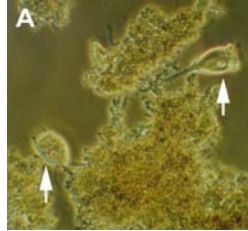


Evolution of Act. Sludge Process

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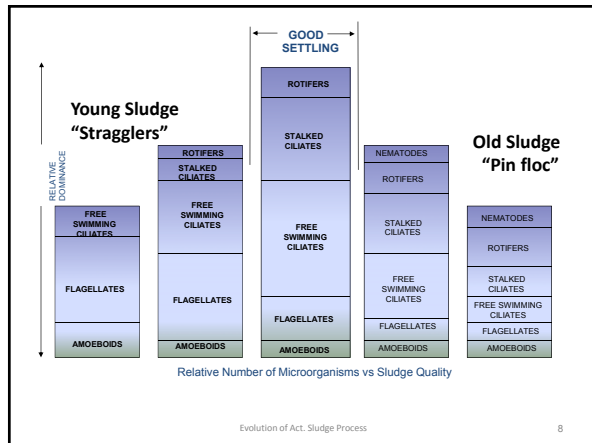
Floc Biology - Indicator of AS Health

- The diversity and activity of organisms found in floc can indicate the health of the biological process.
- An abundance of protozoans such as rotifers indicates healthy situation



Evolution of Act. Sludge Process

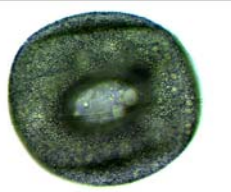
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Evolution of Act. Sludge Process

8

Amoeba



Evolution of Act. Sludge Process

9

Amoeba

- Single-celled protozoans
- Indicative of “young” sludge
- Minimal contribution in WW treatment
- High concentration =
 - BOD shock loading
 - Presence of large amount of particulate matter
 - Lack of DO

Evolution of Act. Sludge Process

10

Flagellate



Evolution of Act. Sludge Process

11

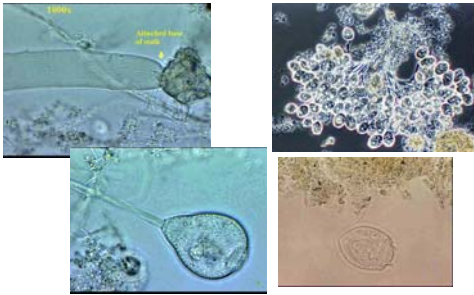
Flagellates

- Nutrient uptake is by absorption
- Peak after amoebae
- Presence -> high soluble food concentration
- Presence indicates WW contains high amount of soluble organic nutrients

Evolution of Act. Sludge Process

12

Ciliates



Evolution of Act. Sludge Process

13

Ciliates

- Free-swimming
 - Peak after flagellates/ correspond to peak in bacteria concentrations
- Stalked
 - Peak after free-swimming
 - Good indicator of settleable sludge

Evolution of Act. Sludge Process

14

Rotifers



Evolution of Act. Sludge Process

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Rotifers

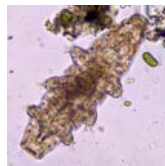
- Number very small
- Appear late in development of activated sludge
- Indicative of “old” sludge
- Sensitive to NH_3 levels, pH, temperature, etc.

Evolution of Act. Sludge Process

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“Water Bears”

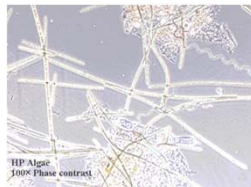
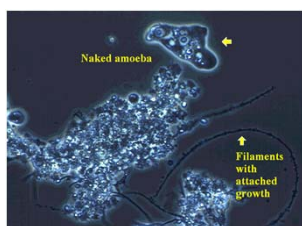
- Tardigrade
- Eight legs
- Can't tolerate NH_3
- Presence in activated sludge biomass indicates absence of NH_3
- Feeds on other protozoa



Evolution of Act. Sludge Process

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Filaments



Evolution of Act. Sludge Process

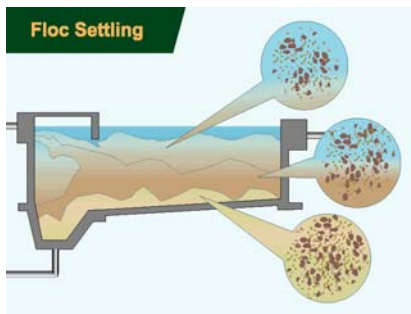
18

Activated Sludge Processes

Observations – Clarifiers

Evolution of Act. Sludge Process

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Evolution of Act. Sludge Process

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Evolution of Act. Sludge Process

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Circular Sedimentation Basin

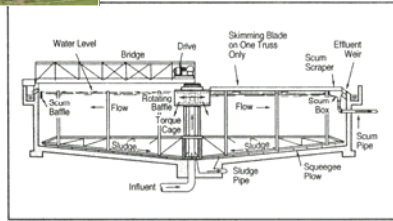


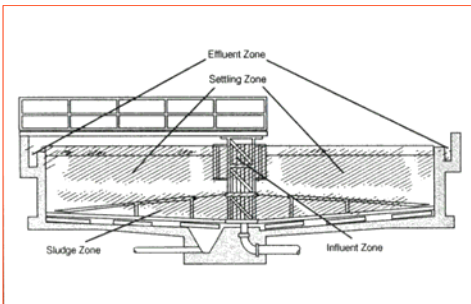
FIGURE S-5 A typical circular sedimentation basin

Courtesy of FMC Corporation, MVS Division

Evolution of Act. Sludge Process

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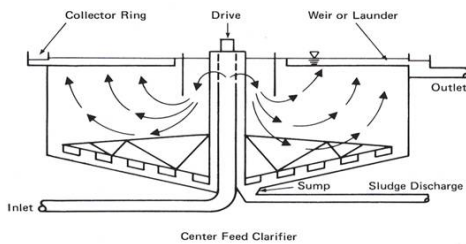
Zones in a Sedimentation Basin



Evolution of Act. Sludge Process

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Circular Sedimentation Schematic



Evolution of Act. Sludge Process

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Typical Operating Parameters — Secondary Clarifiers

Parameter	Operating Range
Detention Time	2.0 to 3.0 hours
Weir Overflow Rate	5,000 to 15,000 gallons per day per lineal foot of weir
Surface Settling Rate or Surface Loading Rate	300 to 1,200 gallons per day per square foot of clarifier surface area
Solids Loading Rate	12 to 30 pounds of solids per day per square foot of clarifier surface area
Source: California State University, Sacramento, "Operation of Wastewater Treatment Plants," Volume 1, 4th ed. 1998.	
thewastewaterblog.com	

Evolution of Act. Sludge Process

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Circular Collectors

- Rotate Clockwise
 - Surface Skimmers for Grease
 - Bottom Flights for Settled Solids
- Solids Removal
 - Pump
 - Gravity
 - Draft Tubes

Evolution of Act. Sludge Process

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Effects of Water Temperature on Clarification

- Warm Water = Improved Clarification
- Cold Water = Reduced Clarification

Evolution of Act. Sludge Process

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Final Clarifier Capacity

- Clarifiers can be hydraulically and/or solids loading limited.
- Design MLSS concentration
- Higher MLSS concentrations may result in clarifier overloading.

Evolution of Act. Sludge Process

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Final Clarifier Operation

- Maintain final clarifier sludge blanket 1 to 2 feet; <30% of clarifier sidewall depth
- If blanket level rises, increase return sludge pumping rate.
- If there is no blanket, reduce return sludge pumping rate.

Evolution of Act. Sludge Process

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Design Criteria

Surface Loading	0.2 – 0.5 gpm/sf; 300 – 800 gpd/sf
Solids Loading	20 – 30 lbs/day/sf
Water Depth	9 – 15 feet
Detention Time	1.5 – 3 hours
Width to Length	1:5
Weir Loading	< 15 gpm/lf

Evolution of Act. Sludge Process

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Improving Clarifier Operation

- Monitor SVI of the Mixed Liquor.
 - Typically should be 150 mL/mg or less.
- If SVI increases due to filamentous bacteria or Nocardia, take corrective action:
 - Eliminate “low DO” (0.4 to 1.0 mg/L) regions of aeration tanks, which breed filaments
 - Increase the F/M ratio of aeration tanks by bypassing primary clarifiers or reducing the number of tanks in service.
 - Chlorinate return sludge to kill filaments.
 - Use spray water system to knock out Nocardia foam on surface.

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Final Clarifier Observations



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Settled Solids Observations



Evolution of Act. Sludge Process

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Settled Solids Observations



Evolution of Act. Sludge Process

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Side-by-Side Comparisons

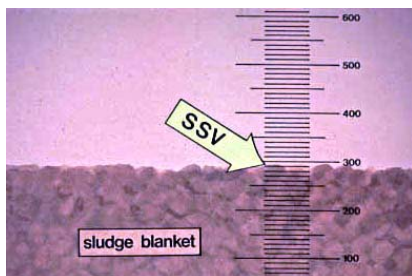


Note the
higher result
in the 1,000
ml graduated
cylinder

Evolution of Act. Sludge Process

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Final Clarifier Observations



Evolution of Act. Sludge Process

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Sludge Volume Index (SVI)

- A numerical expression of the settling characteristics of activated sludge
- SVI is expressed as the ratio of the settled volume in milliliters of activated sludge from a 100-mL sample in 30 minutes divided by the concentration of mixed liquor in milligrams per liter multiplied by 1,000.
- A good settling sludge (textbook value) is 100, but can commonly be between 80-150.

Evolution of Act. Sludge Process

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Mixed Liquor Settling Characteristics

$$SVI = \frac{\text{settled volume of sludge (mL/L)}(10^{-3} \text{ mg/g})}{\text{suspended solids (mg/L)}} = \frac{\text{mL}}{\text{g}}$$

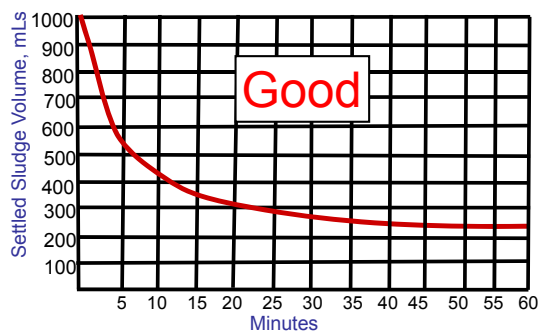
- Place a mixed liquor sample in a 1L or 2L cylinder
- Measure settled volume after 30 min
- Example: mixed liquor sample TSS = 3000 mg/L
- After 30 min, settled volume = 300 mL

$$SVI = \frac{(300 \text{ mL/L})(10^{-3} \text{ mg/g})}{3000 \text{ mg/L}} = \frac{100 \text{ mL}}{\text{g}}$$

- SVI = 100 mL/g – considered good settling sludge
- SVI varies between 50-150 mL/g in properly operating diffused air activated sludge plant

Evolution of Act. Sludge Process

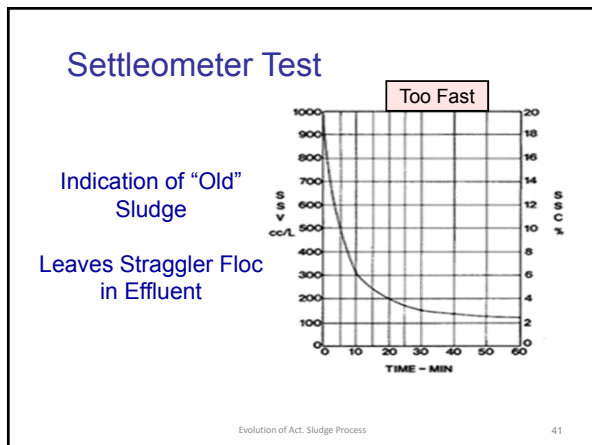
38



Evolution of Act. Sludge Process

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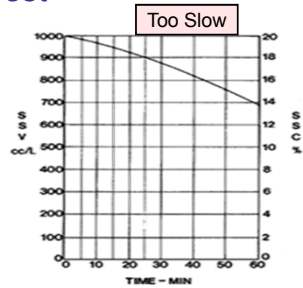




Settleometer Test

Not Compacting
(Bulking)

Solids Washed Out
in High Flows



Evolution of Act. Sludge Process

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Activated Sludge Process

Configurations

Evolution of Act. Sludge Process

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Various Activated Sludge Configurations

- Basin Type:
 - Complete Mix
 - Plug flow reactor
- Air and Feed Options
 - Tapered aeration
 - Step feed
 - Pure oxygen
- Oxidation ditch & Extended Aeration
- Sequencing batch reactor

Evolution of Act. Sludge Process

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Activated Sludge - Extended Aeration

- Stable with intermittent loads
- Long aeration time > 24 hours
- Low organic loadings:
 - 5 to 15 lbs/day/1000 ft³ of aeration
 - Food-to-mass – 0.04 to 0.1
- Solids Residence Time – 20 to 40 days
- Remote facilities:
 - Schools, churches, and mobile home parks
 - Tourist and rest stop facilities

Evolution of Act. Sludge Process

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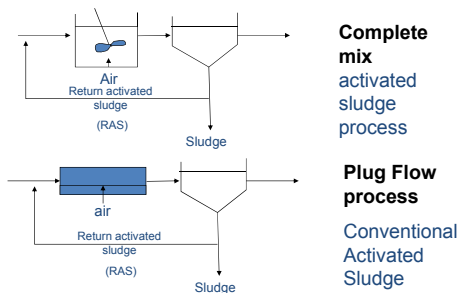
Activated Sludge - Extended Aeration

- MLSS – Range from 2000 to 8000 mg/l.
- Due to the low food/high microbe ratio (F:M ratio), stored food in dead microorganisms is consumed (endogenous respiration)
- Sludge production is much less than other waste activated sludge processes

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Most Common Configurations

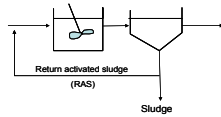


Evolution of Act. Sludge Process

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Complete Mix Activated Sludge

- Advantages:
 - dilutes shock loads
 - relatively simple to operate
- Disadvantages:
 - has low DO and low F/M that encourages growth of filamentous bacteria (sludge bulking!)
 - Less efficient – larger tanks – uniform, low, limited S in reactor

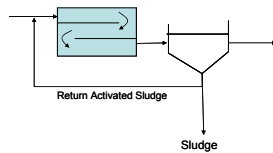


Evolution of Act. Sludge Process

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Activated Sludge - Plug Flow

- Disadvantage
 - Biologically instable when flows vary
- Advantage
 - Avoids “bleed-through” / passage of untreated substrate
 - More efficient - smaller



Evolution of Act. Sludge Process

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Conventional Activated Sludge

- Most common activated sludge process for secondary treatment (cBOD, nBOD, and TSS removal) is plug flow.
- **Plug-flow** basin designed for improved efficiency and small foot-print; tanks are in series
- **Tapered aeration** option to optimize dissolved oxygen supply to match demand in basin.

Evolution of Act. Sludge Process

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Conventional Activated Sludge

- **PLUG FLOW** - Long narrow tank, or a series of several long tanks
- Primary effluent and return activated sludge (RAS) combined at influent of aeration tank
- Dissolved oxygen (DO) demand is highest at the aeration tank entrance; more air (oxygen) is required
- As BOD is depleted, process may successfully operate in the nitrification mode.

Evolution of Act. Sludge Process

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Tapered Aeration

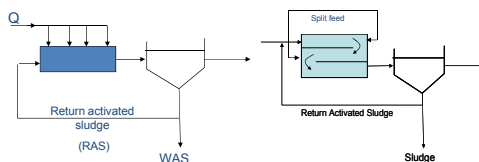
- Deliver more air at the entry points of the aeration tank where the dissolved oxygen demand is at it's highest
- Dissolved oxygen demand is less the exit of the process
- The attempt is to efficiently address oxygen uptake where needed

Evolution of Act. Sludge Process

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Step Feed Activated Sludge

- Flow introduced at 3-4 points in aeration tank to equalize F/M
- High solids inventory – higher MCRT



Evolution of Act. Sludge Process

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Step Feed Activated Sludge

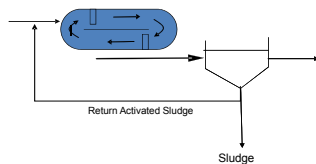
- Advantages of Step-Feed Configuration:
 - Equalize Food/Mass ratio across basin
 - 3 to 5 Passes and influent points
 - Reduces peak oxygen demand – energy efficiency
 - Flexibility to match operating conditions
 - Higher SRT and biomass inventory
 - Lower solids concentration at the end of the aeration tank, lowering the Solids Loading Rate on the final settling tanks

Evolution of Act. Sludge Process

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Oxidation Ditch

- Unidirectional channel flow
- 0.5-1.0 ft/sec velocity keeps sludge in suspension
- Long HRT (24 hrs), long MCRT (>30 days)



Evolution of Act. Sludge Process

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Oxidation Ditch

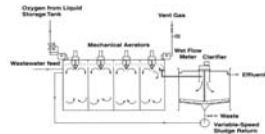


Evolution of Act. Sludge Process

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Pure Oxygen Plug Flow

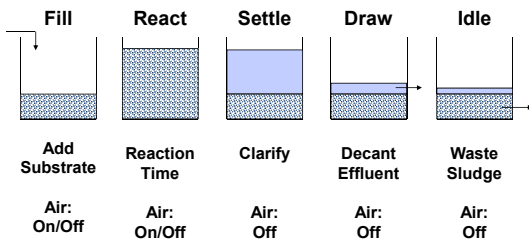
- Staged enclosed reactor
- CO₂ accumulation; lower pH; limits nitrification
- High purity oxygen generated on site
- Reduced space requirement – small footprint



Evolution of Act. Sludge Process

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Sequencing Batch Reactor

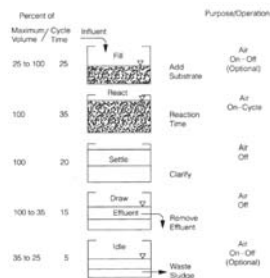


Evolution of Act. Sludge Process

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Sequencing Batch Reactor (SBR)

- One Tank Process
- No Secondary Clarifiers
- Cycles:
 - Fill
 - Aeration
 - Settle
 - Withdrawal
 - Idle



Evolution of Act. Sludge Process

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Activated Sludge Process

BOD Removal to Nitrification

Evolution of Act. Sludge Process

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Forms of Nitrogen

- Ammonia(um) ($\text{NH}_3/\text{NH}_4^+$)
- Organic Nitrogen (Org-N)
- Nitrogen Gas (N_2) ↑
- Nitrite (NO_2^-)
- Nitrate (NO_3^-)

TKN
(Un-oxidized)

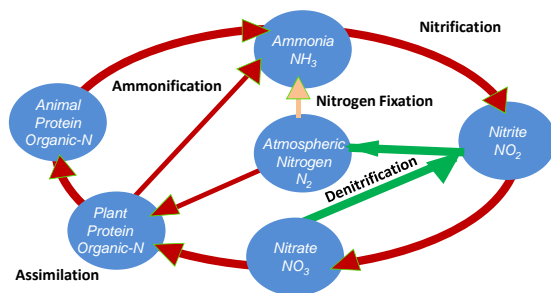
NO_x
(Oxidized)

Total Nitrogen (TN) = TKN + NO_x
TKN = Total Kjeldahl Nitrogen

Evolution of Act. Sludge Process

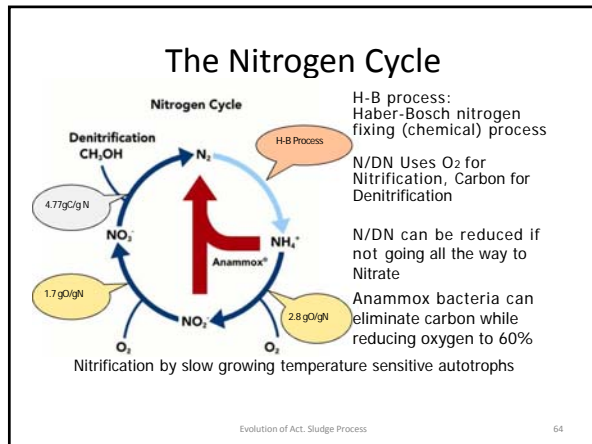
62

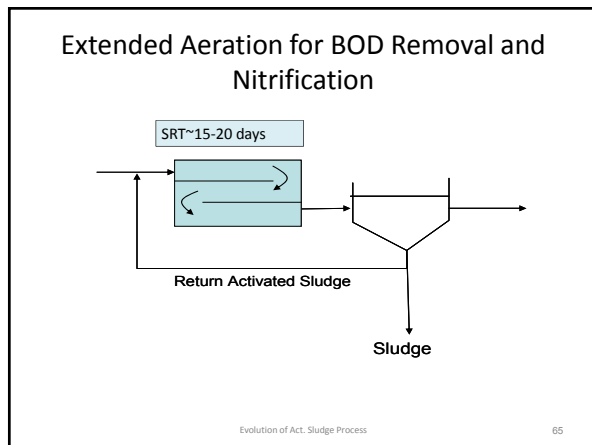
Simplified Nitrogen Cycle in Nature

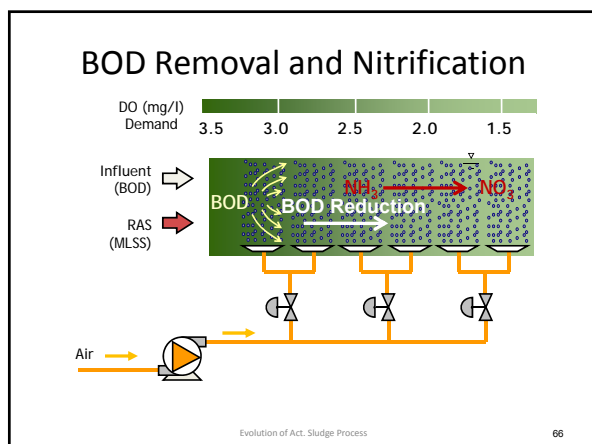


Evolution of Act. Sludge Process

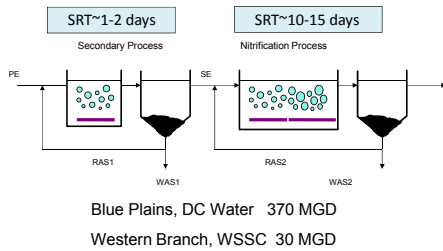
63







Two Sludge System for BOD Removal and Nitrification (1970s)

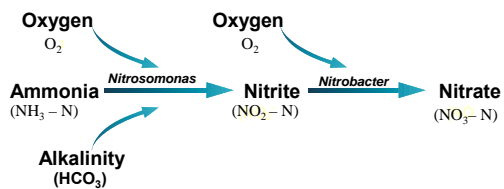


Evolution of Act. Sludge Process

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Nitrification

- For 125 years, nitrification was believed to be solely a two-step process:



Evolution of Act. Sludge Process

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Nitrification

- Two-step nitrification depends on two organisms, which was the basis for hundreds of studies on nitrification in wastewater treatment
- A single microbe capable of catalyzing both nitrification steps may actually conserve energy

Evolution of Act. Sludge Process

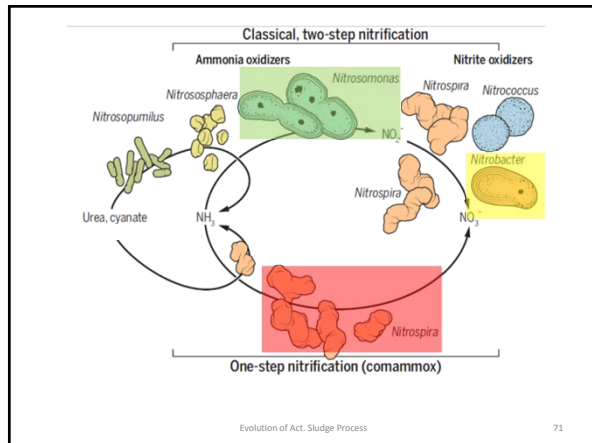
69

Nitrification - Comammox

- **Comammox** (COMplete AMMonia Oxidixer) is the name for a single organism that can convert ammonia into nitrite then nitrate
- Existence of comammox organisms were first predicted in 2006
- In 2015, the presence of such organisms was confirmed within *Nitrospira*
- The Nitrogen cycle has since been updated

Evolution of Act. Sludge Process

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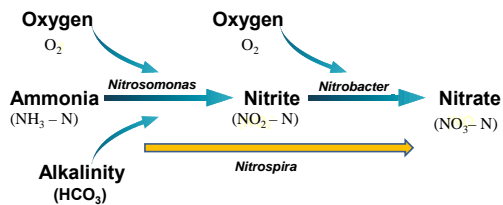


Evolution of Act. Sludge Process

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Nitrification

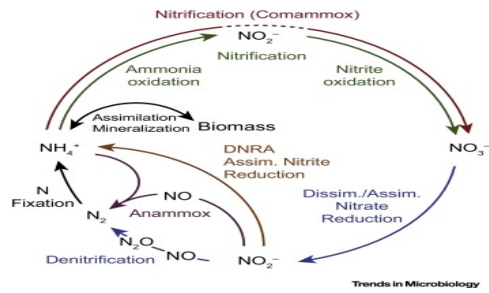
The oxidation (as by bacteria) of ammonia and organic nitrogen to nitrites (NO_2^-) and then further oxidation of nitrites to nitrates (NO_3^-).



Evolution of Act. Sludge Process

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Nitrogen Cycle in Wastewater (2016)



Evolution of Act. Sludge Process

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Nitrification- Operational Problems

• If effluent ammonia-nitrogen is above the goal:

- Verify adequate DO in the aerobic zones.
- Verify adequate alkalinity in the AT effluent.
- Consider if inhibitory compounds could be present.
- If none of the above are true, increase aerobic MCRT.

Evolution of Act. Sludge Process

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Nitrification- Operational Problems

• Ways to raise aerobic MCRT:

- Increase total MCRT by reducing sludge wasting, but do not allow rising MLSS to exceed clarifier capacity.
- Increase percent volatiles (MLVSS) without increasing total MLSS by reducing the amount of inerts entering system through chemical feeds and sidestream loads (i.e. from septage or sludge thickening/digestion).
- Increase MCRT without raising MLSS by bringing more aeration tanks or RBCs on-line.
- Increase aerobic MCRT without raising total MCRT by operating switch zones in the aerobic mode

Evolution of Act. Sludge Process

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Nitrification Problems

Possible Causes	Solution
Insufficient MCRT	Increase MCRT to establish nitrification by reducing sludge wasting
Insufficient DO in aerobic zone (~ 2.0 mg/L goal)	Increase aeration by adjusting air valves, increasing blower output, or turning on another blower.
Insufficient alkalinity	Add supplemental alkalinity to maintain 50 mg / L as CaCO ₃ in effluent
Chemical inhibition of nitrifiers	Trace source of improper discharge of nitrification inhibitors and eliminate at source

Evolution of Act. Sludge Process

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Activated Sludge Process

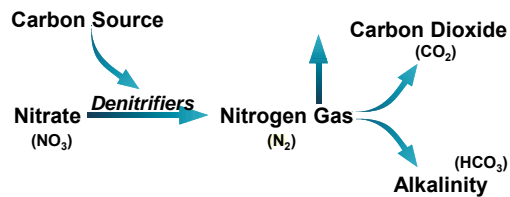
Denitrification

Evolution of Act. Sludge Process

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Denitrification

Reduction of nitrates or nitrites commonly by bacteria usually resulting in the escape of nitrogen in the air.



Evolution of Act. Sludge Process

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Denitrification Requirements

- Nitrification to produce nitrite/nitrate
- Anoxic zones with low/no DO
 - Baffling and zone segregation
 - Minimize DO carryover from aerated zones
- Readily biodegradable carbon (rbCOD)
 - Raw Influent BOD (~ 5-6 lbs BOD/lb NO₃-N denitrified)



Evolution of Act. Sludge Process

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Denitrification Requirements

- Impact on Oxygen and Alkalinity:
 - Alkalinity is *produced* in Denitrification
 - 50% of alkalinity consumed in Nitrification is recovered in denitrification
- Nitrification:
 - $\text{NH}_4^+ + 2 \text{O}_2 \rightarrow \text{NO}_3^- + 2\text{H}^+ + \text{H}_2\text{O}$
- Denitrification:
 - $6\text{NO}_3^- + 5\text{CH}_3\text{OH} \rightarrow 3\text{N}_2 + 5\text{CO}_2 + 7\text{H}_2\text{O} + 6\text{OH}^-$

Evolution of Act. Sludge Process

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Conditions in the Anoxic Zone

DO less than 0.1 mg/l

No aeration

Low aeration

Cyclical Aeration

Carbon source

Primary Effluent

Endogenous

Methanol

Mixing

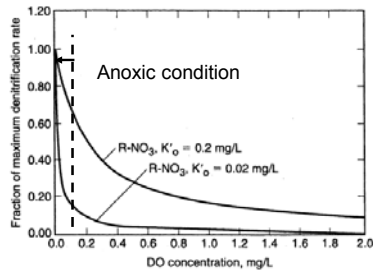
Submersible mixers

Vertical mixers

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Reduction in rate of Denite as a function of D.O.
(K'_o is oxygen inhibition constant)



Evolution of Act. Sludge Process

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Inhibition of Denite Process

- Environmental Conditions
 - pH
 - Temperature
 - **Aerobic Conditions! Keep DO < 0.2 mg/L**
- Insufficient amount of rbCOD (Carbon Substrate).
- Presence of Chemical Inhibitors:
 - Substrates, intermediates, and products of denitrification
 - Synthetic organic chemicals
 - Heavy metals - Hg, Ni, Pb, etc.

Evolution of Act. Sludge Process

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Denitrification

Note: (Almost) all nitrates returned to the anoxic zones should be denitrified

The “goal” $\text{NO}_3\text{-N}$ concentration in the effluent from the last anoxic zone should be between 0 and 0.5 mg/L.

Evolution of Act. Sludge Process

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Carbon for Denitrification

- Influent WW Carbon
 - Utilized in first anoxic zone
 - EBPR can compete for carbon
 - Limited carbon available for secondary anoxic zones – and effective denite
- Endogenous Carbon
 - Slow kinetics – limited denite in post-anoxic zones
- Supplemental Carbon
 - Methanol typically used
 - But requires methylotrophic population!
 - Alternatives to methanol – ethanol, acetic acid, glycerin, sugars, mono-propylene glycol, proprietary products

Evolution of Act. Sludge Process

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Other Carbon Sources

- Alcohols
 - Methanol
 - Ethanol
- Glycerol/glycerin – (Biodiesel by-products)
- Acetates - (Acetic acid, sodium acetate)
- Carbohydrates - (Sucrose, sugar water, corn syrup)
- MicroC™ – (Carbohydrate, glycerin, alcohol based blends)

Evolution of Act. Sludge Process

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Carbon for Denitrification

- If using methanol – may not have adequate methylotrophic population
 - Need well controlled anoxic volume
 - Methylotrophs may require acclimation time
 - Methylotrophs are believed to be more sensitive to temperature
- Methanol is typically more sensitive to pH and may not be effective in very cold weather
 - Change carbon source – ethanol or glycerin
- Denitrification batch tests
 - Specific denitrification rates (SDNRs) – different carbon sources

Evolution of Act. Sludge Process

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Inhibition by specific Chemicals

- Strong Inhibitors
 - Acetylene (C_2H_2)
 - Sulfide (S^{2-})
 - Chlorate (ClO_3^-)
 - Heavy metals
 - Cyanide (CN^-) and Azide (N_3^-)

Evolution of Act. Sludge Process

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Denitrification Problems

Possible Causes	Solution
Not enough nitrates being returned to anoxic zone	Increase nitrate recycle pump speed
Not enough BOD entering anoxic zone	- Bypass primary clarifiers, or - Add supplemental carbon (for example, methanol) to anoxic zone
BOD entering the anoxic zone breaks down too slowly	Add readily available carbon source such as methanol to anoxic zone or increase the anoxic zone hydraulic retention time
High DO in the anoxic zone	Try to limit backmixing of air from the aerobic zones or decreasing the DO in the AT influent. Decrease nitrate recycle rate if necessary.

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Activated Sludge Process

Nitrification to BNR

Evolution of Act. Sludge Process

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Nitrogen Removal - Basics

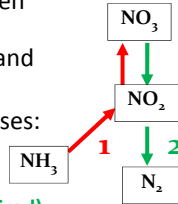
Nitrification + **Denitrification** = Nitrogen Removal

- BNR/ENR converts TKN nitrogen (primarily ammonia) in wastewater to nitrite/nitrate and ultimately **nitrogen gas**

- BNR/ENR requires two processes:

–1: **Nitrification** (O_2 & HCO_3^- required)

–2: **Denitrification** (Carbon required)

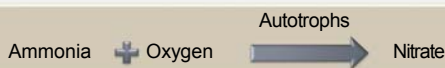


Evolution of Act. Sludge Process

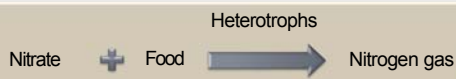
91

Nitrification-Denitrification

Nitrification improves oxygen in receiving waters:



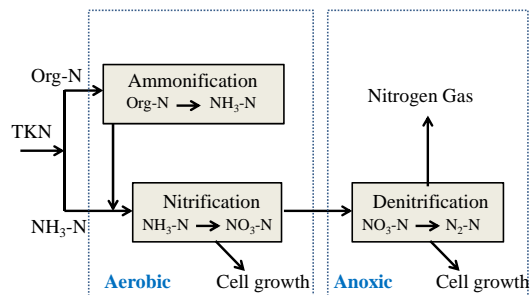
Denitrification removes nitrogen:



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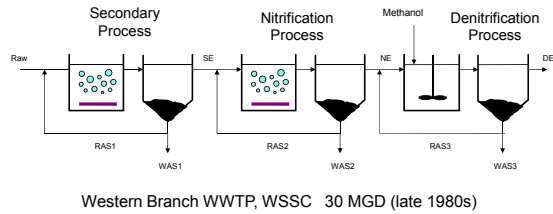
Nitrification-Denitrification



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Three Stage System for BOD Removal and Nitrogen Removal to <3 mg/L

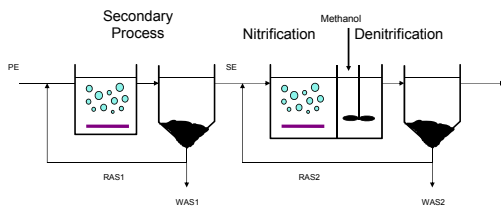


Western Branch WWTP, WSSC 30 MGD (late 1980s)

Evolution of Act. Sludge Process

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Two Sludge System for BOD Removal and Nitrogen Removal to <5 mg/L

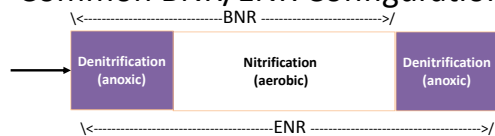


Blue Plains, DC Water 370 MGD (beginning early 1990s)

Evolution of Act. Sludge Process

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Common BNR/ENR Configurations



- BNR:
 - Modified Ludzack-Ettinger (MLE)
 - Anaerobic/Anoxic/Oxic (A2O)
 - University of Cape Town Process (UCT)
- ENR:
 - Enhanced MLE/4-stage Bardenpho
 - MLE with Denitrification Filter

Evolution of Act. Sludge Process

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Nutrient Removal

- Nitrification (*Nitrosomonas* and *Nitrobacter*)
 $\text{NH}_3 + \text{O}_2 \rightarrow \text{NO}_2^- \rightarrow \text{NO}_3^-$
- Denitrification
 $\text{NO}_3^- + \text{organics} \rightarrow \text{CO}_2 + \text{N}_2$
- BNR Process – MLE
- FeCl_3 for TP removal

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Modified Ludzack-Ettinger BNR Process

Denitrification-Nitrification with Nitrate Recycle

STAGE	PURPOSE
Anoxic	BOD Removal, Denitrification, and Nitrogen gas release
Aerobic (Oxic)	Nitrification zone

Evolution of Act. Sludge Process

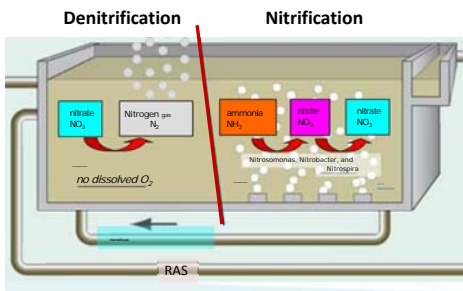
98

Denitrification/Nitrification Layout

Evolution of Act. Sludge Process

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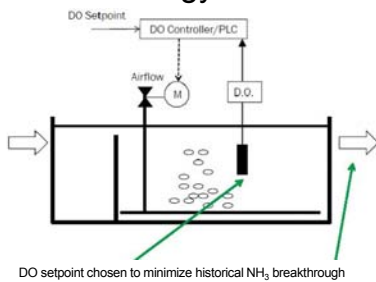
Biological Nitrogen Removal



Evolution of Act. Sludge Process

100

Typical Aeration Basin Control Strategy - DO



Evolution of Act. Sludge Process

101

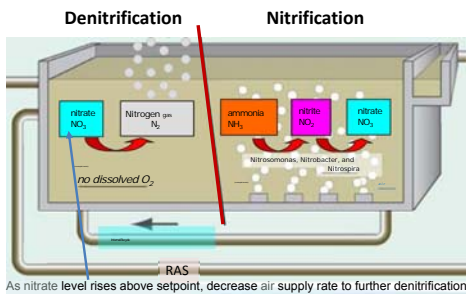
Objective of Ammonia based Aeration control

- Aeration is limited to:
 - Prevent complete nitrification
 - Reduce effluent ammonia peaks
- Potential benefits include:
 - Decreased energy expenses (for aeration)
 - Possibly increased denitrification with less supplemental carbon addition
 - Possibly improved Bio-P removal

Evolution of Act. Sludge Process

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Biological Nitrogen Removal

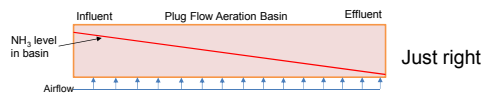


Evolution of Act. Sludge Process

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Ammonia-Based DO Control

- Operator selects effluent ammonia setpoint
 - Complete nitrification, NH₃-N ~ 0.1 mg/L
 - Incomplete nitrification, NH₃-N ≤ 1.0 to 2.0 mg/L

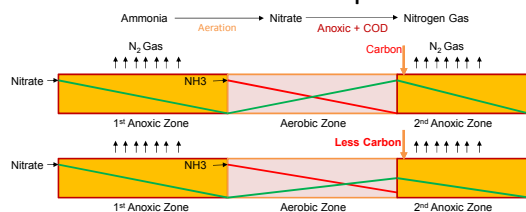


- When effluent ammonia is greater than setpoint, controller increases DO
- When effluent ammonia is below setpoint, controller decreases DO

Evolution of Act. Sludge Process

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Benefit of Ammonia-Based DO Control Reduced Carbon Requirement



Evolution of Act. Sludge Process

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Advanced (Tertiary) Treatment

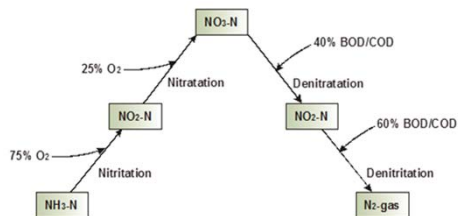
- Nutrient Removal with Activated Sludge
 - Total Nitrogen (TN) removal
 - Nitrification
 - Denitrification
 - BNR and ENR technologies
 - EPA Model (Nitrification/Denitrification)
 - Modified Ludzack-Ettinger – MLE (Denitrification/Nitrification)
 - Enhanced MLE/Bardenpho – MLE with post denitrification

Evolution of Act. Sludge Process

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Simultaneous Nitrification and Denitrification (SNDN)

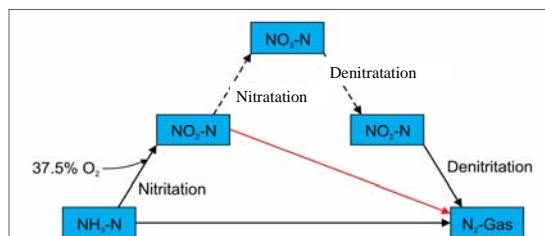
Traditional pathway of biological nitrogen removal



Evolution of Act. Sludge Process

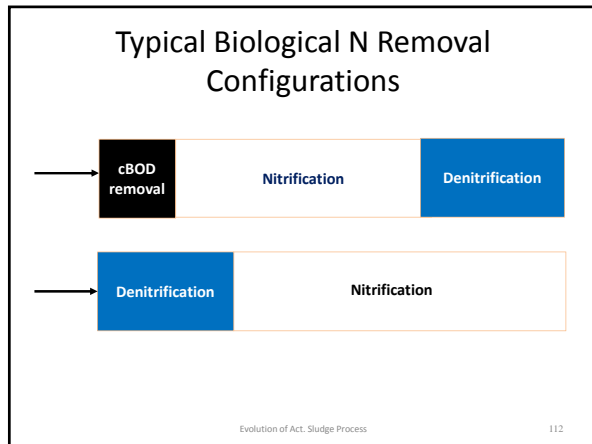
110

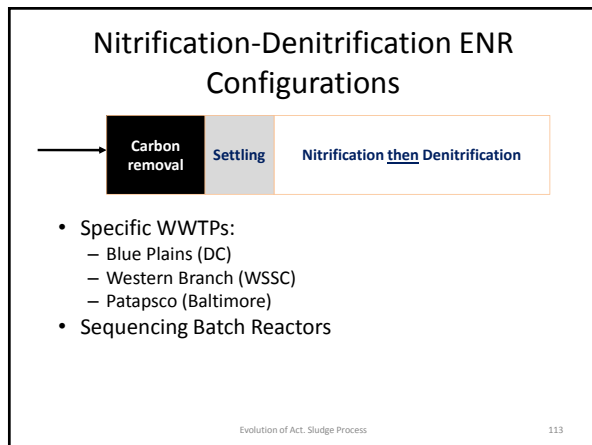
Deammonification "ANAMMOX"

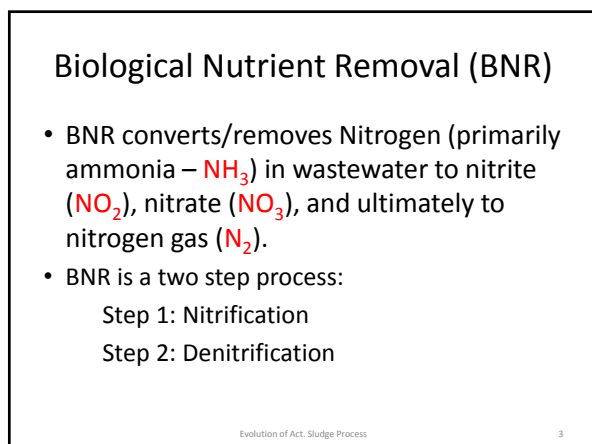


Evolution of Act. Sludge Process

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Milestones

- 1954 Wuhrman proposes 2-stage, aerobic - anoxic process
- 1957 Davidson proposes 2-stage, anaerobic - aerobic Process
- 1962 Ludzack and Ettinger propose 2-stage, anoxic – aerobic process
- 1967 Leven patents Phostrip®, a sidestream phosphorus removal process

Evolution of Act. Sludge Process

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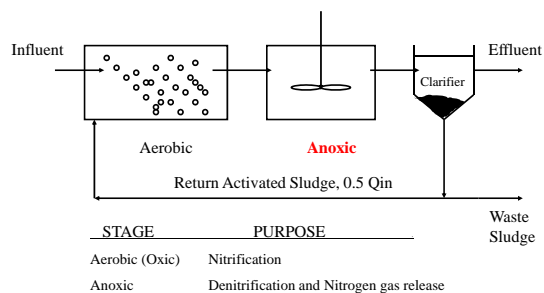
Milestones

- 1968 Barth proposes 3-sludge, activated sludge process for nutrient removal
- 1970 Savage patents denitrification filter
- 1973 Barnard in South Africa develops the Modified Ludzack-Ettinger process, which becomes the standard for the wastewater industry

Evolution of Act. Sludge Process

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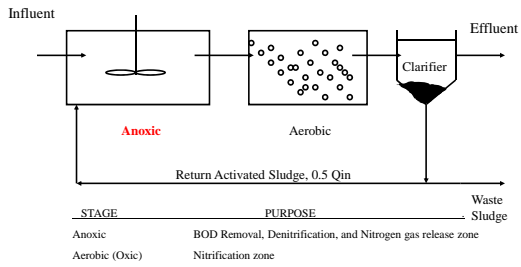
Two Stage Wuhrmann BNR Process



Evolution of Act. Sludge Process

117

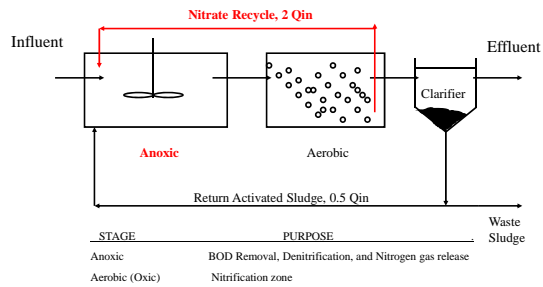
Two Stage Ludzack-Ettinger BNR Process



Evolution of Act. Sludge Process

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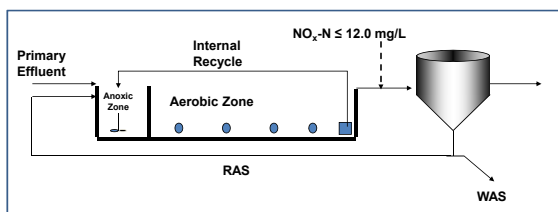
Modified Ludzack-Ettinger BNR Process



Evolution of Act. Sludge Process

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Modified Ludzack-Ettinger (MLE) Configuration



Evolution of Act. Sludge Process

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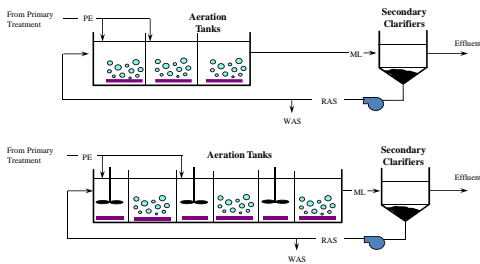
Modified Ludzack-Ettinger - MLE



Evolution of Act. Sludge Process

121

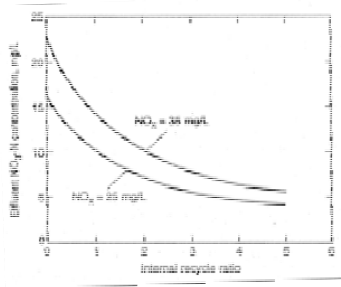
Step Feed Process



Evolution of Act. Sludge Process

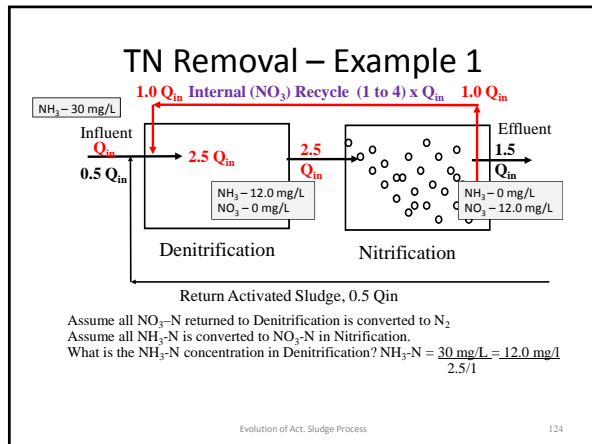
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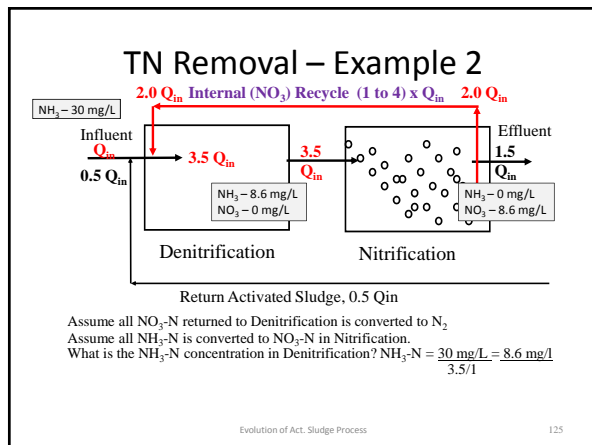
Impact of Internal Recycle on BNR Effluent TN

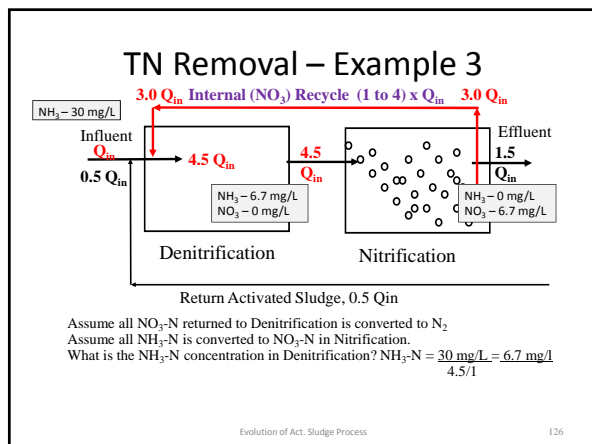


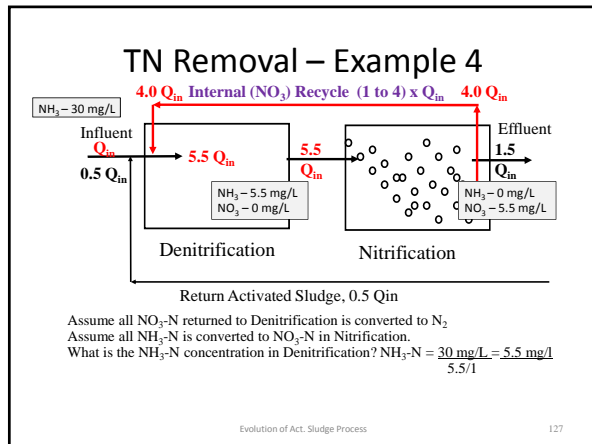
Evolution of Act. Sludge Process

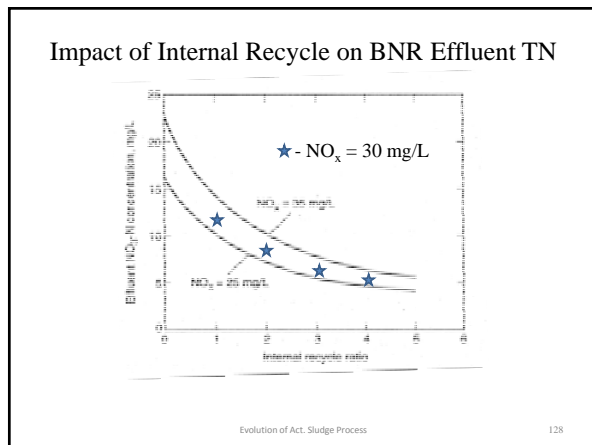
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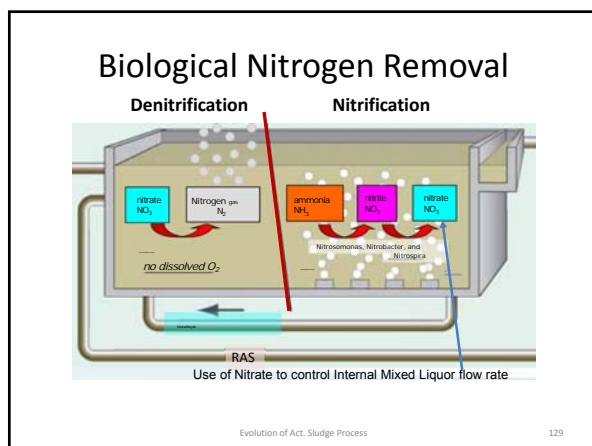




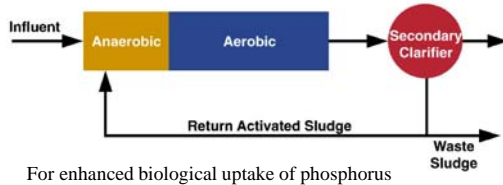








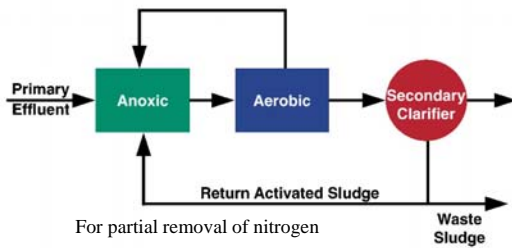
AO



Evolution of Act. Sludge Process

130

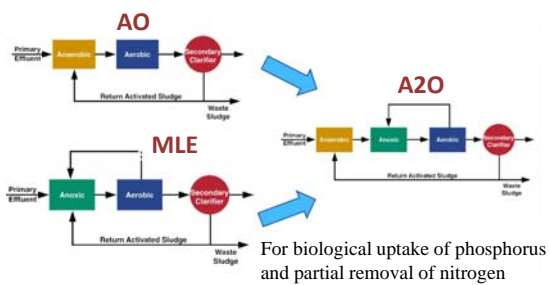
Modified Ludzack-Ettinger - MLE



Evolution of Act. Sludge Process

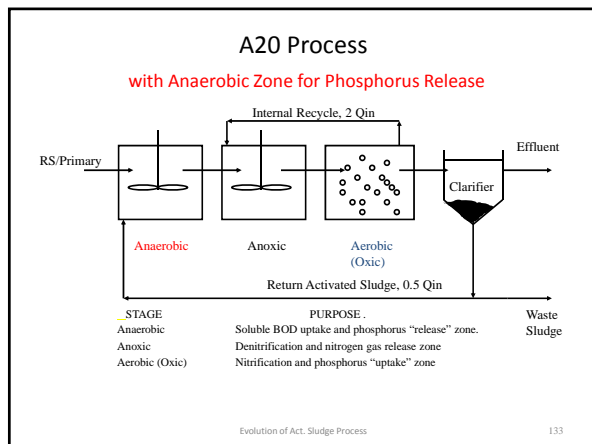
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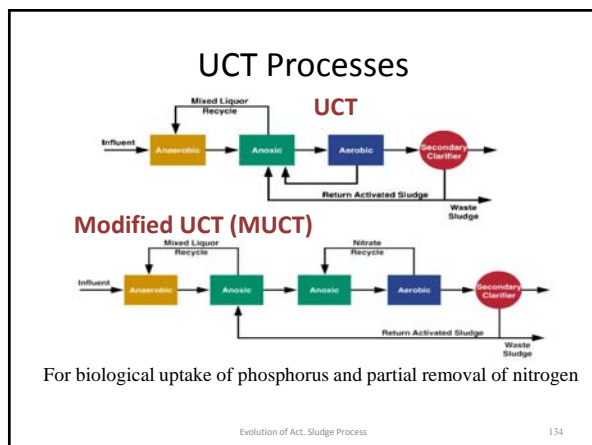
AO plus MLE = A2O



Evolution of Act. Sludge Process

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Historical View of BNR

- Recent efforts for nutrient removal for WWTPs with limited space for expansion has lead to:
 - Sequencing Biological Reactors (SBRs)
 - Membrane reactors
 - Side-stream treatment for phosphorus removal:
 - Struvite precipitation
 - Side-stream treatment for ammonia removal:
 - Deammonification with ANAMMOX

Evolution of Act. Sludge Process 135

BNR Processes

Process	Nitrogen	Phosphorus	Comments
MLE	Good	None	- Moderate basin volume
Step Feed	Good	None	- No nitrate recycle
SBR	Moderate	Inconsistent	- No nitrate recycle
A2O	Good	Good	- Moderate basin volume - Sensitive to DO in return
Oxidation Ditch	Excellent	Good	- Long HRT and SRT - Tight DO controls necessary

Evolution of Act. Sludge Process

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High DO in the Anoxic Zones

- High DO in the anoxic zones may be more of a problem during the winter because more DO can be absorbed by colder water and biological kinetics are reduced.
- Lower the nitrate recycle rate in the winter if necessary

Evolution of Act. Sludge Process

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Denitrification

- **If effluent nitrate-nitrogen is above the goal:**
 - Verify nitrate recycle pumps are running.
 - Check nitrate recycle pump speed.
 - Verify very low DO in the anoxic zones.
 - Consider if low influent BOD or slowly degradable influent BOD could be inhibiting the process.

Evolution of Act. Sludge Process

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Activated Sludge Process

BNR to ENR

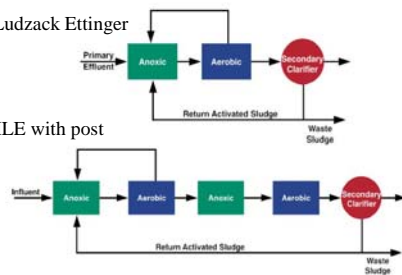
Evolution of Act. Sludge Process

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Example of BNR to ENR

Modified Ludzack Ettinger
- MLE

Enhanced MLE with post
anoxic zone



Evolution of Act. Sludge Process

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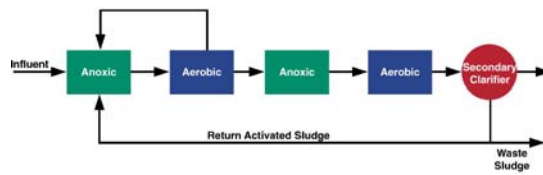
Milestones

- 1975 Barnard patents Bardenpho® process
- 1976 Specter patents AO® and A2O® processes
- 1977 Jervis develops fluidized bed denitrification reactor
- 1980 University of Cape Town (UCT) process developed

Evolution of Act. Sludge Process

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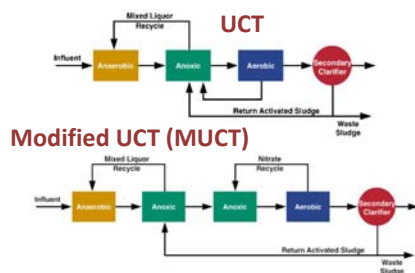
Bardenpho (Enhanced Modified Ludzack Ettinger)



Evolution of Act. Sludge Process

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UCT Processes



Evolution of Act. Sludge Process

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Anoxic Zone

- In the MUCT process, baffling or separate tanks are set up in the anoxic reactor.
 - First reactor (primary) receives underflow from settling tank
 - MLSS from first reactor is recycled to the anaerobic tank
 - Second anoxic reactor receives mixed liquor from aerobic tank

Evolution of Act. Sludge Process

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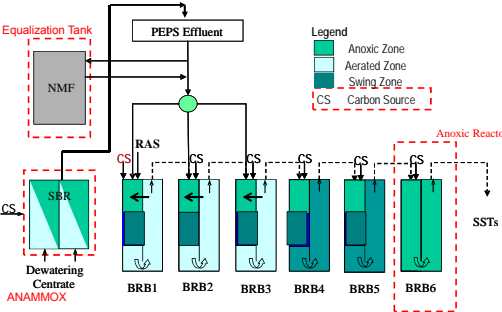
Enhanced Nutrient Removal (ENR)

- For WWTPs to upgrade from BNR to ENR, and satisfy new LOT requirements for nitrogen removal, an additional post-denitrification stage is required; for example:
 - MLE + post anoxic
 - MLE + Denit Filter
 - Step feed + post anoxic
 - Step feed + Denit Filter

Evolution of Act. Sludge Process

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AlexRenew Step Feed Facility



Evolution of Act. Sludge Process

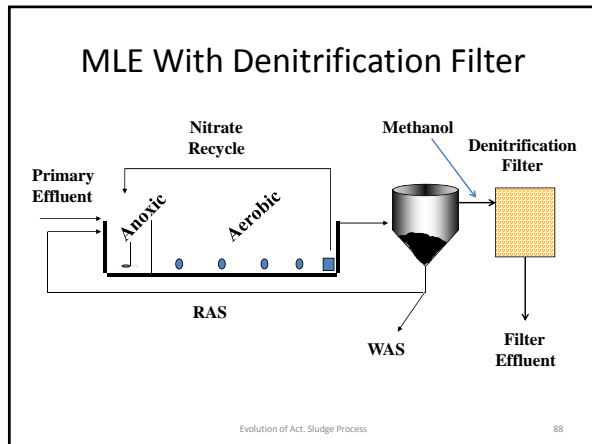
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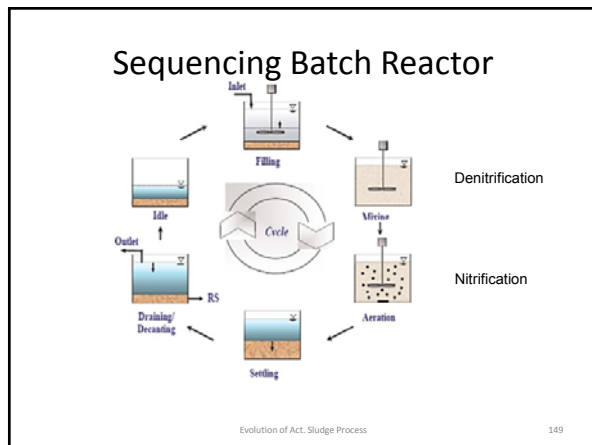
ENR Processes

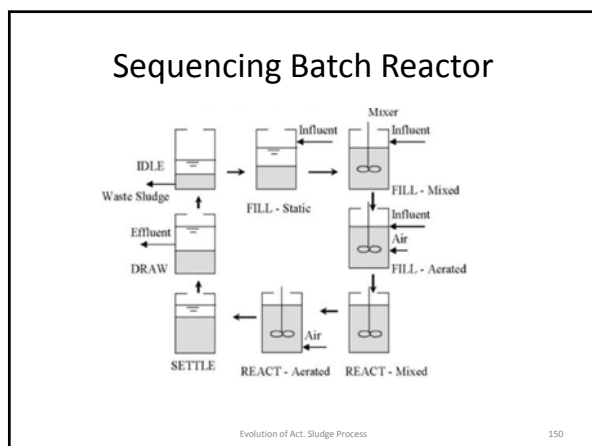
Process	Nitrogen	Phosphorus	Comments
Enhanced MLE (Bardenpho)	Excellent	None	- Large basin volume - Need for methanol
Modified UCT	Good	Excellent	- Separate anoxic zone for RAS - Several nitrate recycle streams - Increased complexity
5-stage Bardenpho	Excellent	Good	- Larger reactor volume - Need for methanol
Oxidation Ditch	Excellent	Good	- Long HRT and SRT - Tight DO controls necessary

Evolution of Act. Sludge Process

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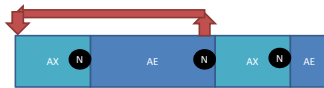






Nutrient-Paced Mode is Most Accurate

- Requires nitrate probes/analyzers
 - Locate in/out of anoxic zone and filters
- Operator input
 - Effluent nitrate setpoint (mg/L)

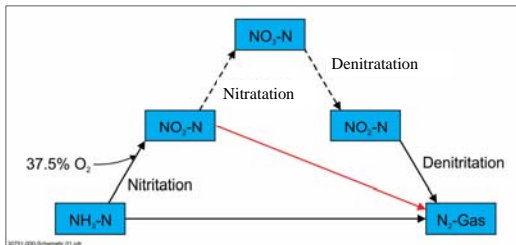


Typical probe locations

Evolution of Act. Sludge Process

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Nitrification/Denitrification “ANAMMOX”

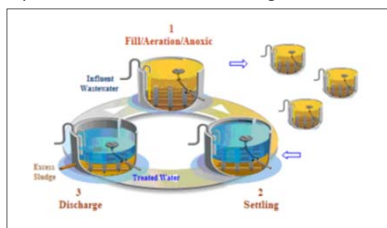


Evolution of Act. Sludge Process

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SBR-type Anammox Process

- Three 8-hour Cycles per day using special bacteria
- Hampton Roads and Alexandria, Virginia



Evolution of Act. Sludge Process

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Advantages and Disadvantages of BNR/ENR

- **Advantages**
 - No chemicals
 - No additional chemical sludge
 - retrofits well with any activated sludge process
 - Additional benefit of nitrogen removal
- **Disadvantages**
 - Except for Phostrip, phosphorus removal is a function of BOD:TP ratio
 - Not easily retrofitted to fixed film facilities
 - Standby chemical addition may be necessary as a backup

Evolution of Act. Sludge Process

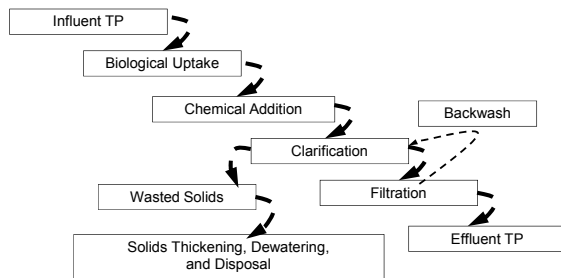
154

Phosphorus Removal Processes

Evolution of Act. Sludge Process

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Phosphorus Removal



Evolution of Act. Sludge Process

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Phosphorus Removal - Basics

1. Chemical precipitation – two mechanisms:

- **Co-Precipitation** (Remove TP ~ 0.5 mg/l)
 - $2\text{Al} + 3\text{OH} + \text{PO}_4 \rightarrow 2\text{Al}(\text{OH})_3\text{PO}_4 \downarrow$
- **Adsorption** (Remove TP < 0.5 mg/l)
 - $x(\text{Al} + 3\text{OH}) \rightarrow x(\text{Al}(\text{OH})_3) \downarrow$
 - $x(\text{Al}(\text{OH})_3) \downarrow + \text{PO}_4 \rightarrow x(\text{Al}(\text{OH})_3)\text{PO}_4 \downarrow$
 - $x > 2$; more chemical required as PO_4 levels drop
- Both reactions form Metal-Hydroxide-Phosphate sludge

2. Biological Uptake

- Conventional/background uptake (2 to 3%)
- Luxury/excess uptake (BNR/ENR - 3 to 6%)

Evolution of Act. Sludge Process

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Phosphorus Removal Options

- Source control – bans on phosphates in detergents
- Physical removal of particulate phosphorus during sedimentation and filtration
- Biological uptake
- Chemical addition with alum or FeCl_3

Evolution of Act. Sludge Process

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Phosphate Bans in Detergents

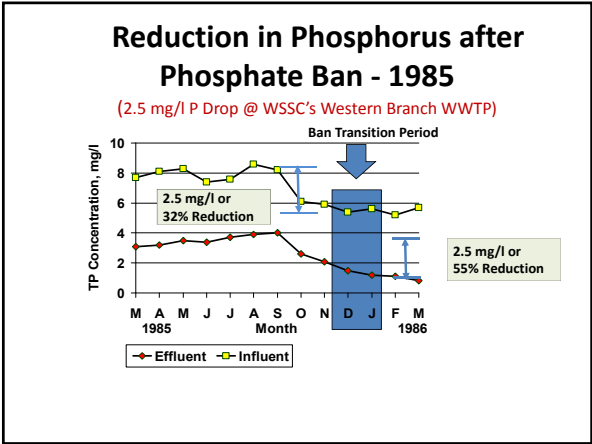
In the mid-1980's, Maryland, Pennsylvania, Virginia, and the District of Columbia instituted bans on phosphates in laundry detergents.

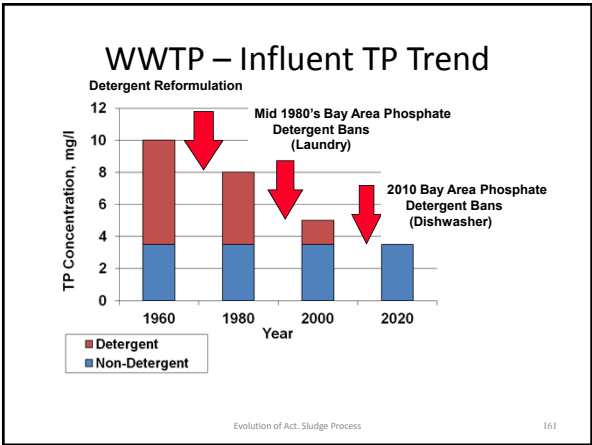


Nearly 25 years later, a second regional ban became effective on phosphates in automatic dishwasher detergents.

Evolution of Act. Sludge Process

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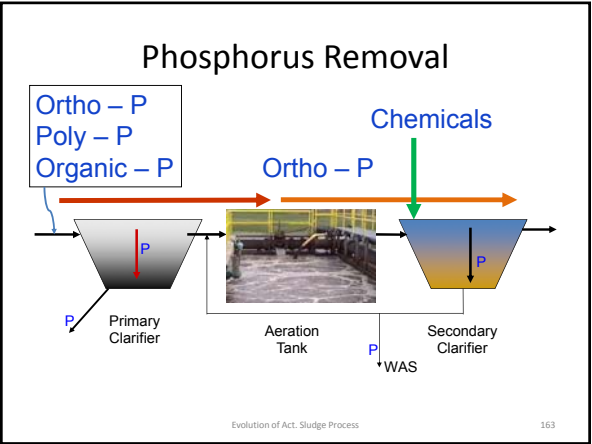




Background Uptake

- Conventional Biological Uptake
 - To satisfy biological needs
- Excess Biological uptake
 - Stress induced
 - Anaerobic zones
 - Release of phosphorus under anaerobic conditions
 - Uptake of phosphorus under aerobic conditions

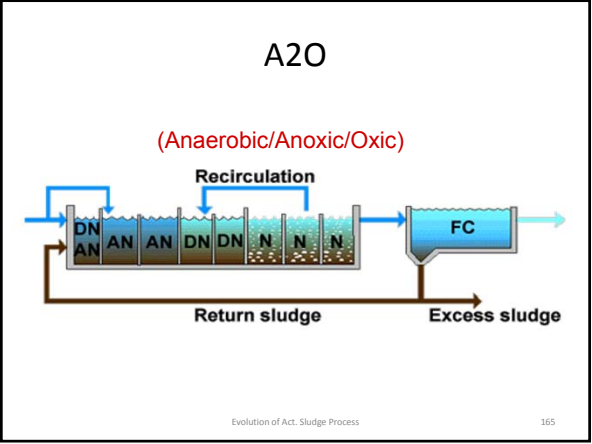
Evolution of Act. Sludge Process 162



Biological Phosphorus Removal Concept

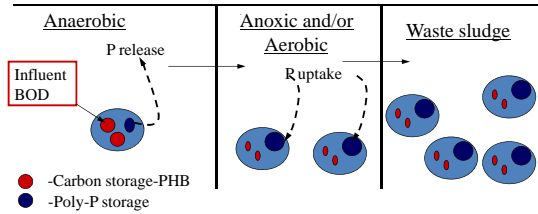
- Modify treatment system so that waste activated sludge contains higher than normal concentrations of phosphorus.
- 2 to 3 times as much phosphorus removed in BNR Systems
 - Conventional - 1 to 3%
 - BNR Systems - 2 to 6%

Evolution of Act. Sludge Process 164



Biological TP Uptake

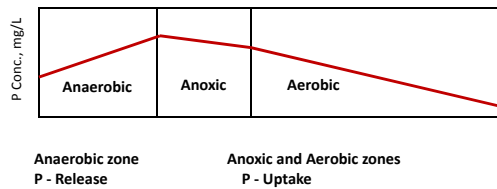
P is removed by phosphorus accumulating organisms (PAOs) and exits system in waste sludge



Evolution of Act. Sludge Process

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Phosphorus Profile – A2O



Evolution of Act. Sludge Process

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Phosphorus Removal with Chemicals

Chemical precipitation – two mechanisms:

- **Co-Precipitation** (Remove TP ~ 0.5 mg/l)
 - $2Al + 3OH + PO_4 \rightarrow 2Al(OH)_3 \cdot PO_4 \downarrow$
- **Adsorption** (Remove TP < 0.5 mg/l)
 - $x(Al + 3OH) \rightarrow x(Al(OH)_3) \downarrow$
 - $x(Al(OH)_3) \downarrow + PO_4 \rightarrow x(Al(OH)_3 \cdot PO_4) \downarrow$
 - $x > 2$; more chemical required as PO_4 levels drop
- Both reactions form Metal (Al or Fe)-Phosphate-Hydroxide sludge

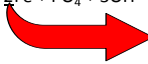
Evolution of Act. Sludge Process

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Simplified Iron Reactions

- $\text{FeCl}_3 + \text{PO}_4^{-3} \rightarrow \text{FePO}_4 + 3\text{Cl}^{-1}$
- $\text{FeCl}_3 + 3\text{HCO}_3^{-1} \rightarrow \text{Fe(OH)}_3 + 3\text{CO}_2 + 3\text{Cl}^{-1}$

- Simplified: $\text{Fe} + \text{PO}_4 \rightarrow \text{FePO}_4$
 $\text{Fe} + 3\text{OH} \rightarrow \text{Fe(OH)}_3$

- Combined:
 $2\text{Fe} + \text{PO}_4 + 3\text{OH} \rightarrow 2\text{FePO}_4(\text{OH})_3 \text{ Complex}$ ↓
 (Mole Ratio = 2.0)

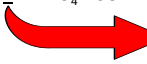
Evolution of Act. Sludge Process

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Simplified Aluminum Reactions

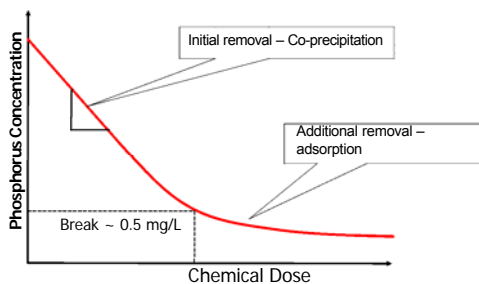
- $\text{Al}_2(\text{SO}_4)_3 \cdot 14\text{H}_2\text{O} + 2\text{PO}_4^{-3} \rightarrow 2\text{AlPO}_4 + 3\text{SO}_4^{-2} + 14\text{H}_2\text{O}$
- $\text{Al}_2(\text{SO}_4)_3 \cdot 14\text{H}_2\text{O} + 6\text{HCO}_3^{-1} \rightarrow 2\text{Al(OH)}_3 + 6\text{CO}_2 + 14\text{H}_2$

- Simplified: $\text{Al} + \text{PO}_4 \rightarrow \text{AlPO}_4$
 $\text{Al} + 3\text{OH} \rightarrow \text{Al(OH)}_3$

- Combined:
 $2\text{Al} + \text{PO}_4 + 3\text{OH} \rightarrow 2\text{AlPO}_4(\text{OH})_3 \text{ Complex}$ ↓
 (Mole Ratio = 2.0)

Evolution of Act. Sludge Process

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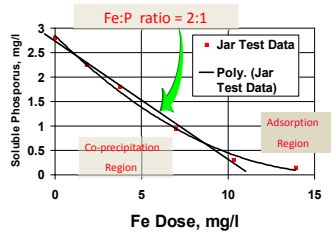


Evolution of Act. Sludge Process

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Phosphorus Removed with FeCl_3

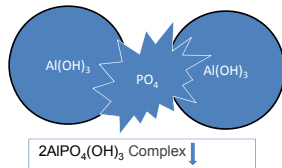
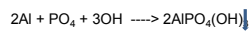
Blue Plains - June 1977



Evolution of Act. Sludge Process

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Co-precipitation Model

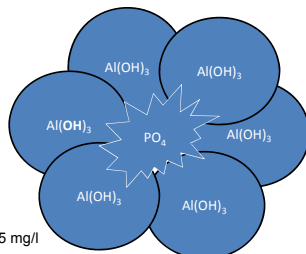


- ✓ For PO_4 concentrations > 0.5 mg/l
- ✓ Stoichiometric chemical reactions
- ✓ Mole ratio – 1.5 to 2.0

Evolution of Act. Sludge Process

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Adsorption Model



- ✓ For PO_4 concentrations < 0.5 mg/l
- ✓ More chemical needed
- ✓ Mole ratio – 2.0 to 10.0

Evolution of Act. Sludge Process

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Typical Chemicals Used To Precipitate Phosphorus

- Alum - $\text{Al}_2(\text{SO}_4)_3 \cdot 14\text{H}_2\text{O}$
- Ferric Chloride - FeCl_3
- Poly-Aluminum Chloride (PACl)
- Pickle Liquor - FeSO_4
- Sodium Aluminate - $\text{Na}_2\text{Al}_2\text{O}_4$
- Lime, pH > 10

Evolution of Act. Sludge Process

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Chemicals used for Phosphorus Precipitation

Chemical	Formula	Removal mechanism	Effect on pH
Ferric Chloride	FeCl_3 M.W. = 162.3	Metal hydroxides	Removes alkalinity
Aluminum Sulfate (Alum)	$\text{Al}_2(\text{SO}_4)_3 \cdot 14.3(\text{H}_2\text{O})$ M.W. = 599.4	Metal hydroxides	Removes alkalinity
Ferrous sulfate (pickle liquor)	Fe_2SO_4	Metal hydroxides	Removes alkalinity
Poly Aluminum Chloride	$\text{Al}_n\text{Cl}_{(3n-m)}(\text{OH})_m$ $\text{Al}_{12}\text{Cl}_{24}(\text{OH})_{24}$	Metal hydroxides	none
Lime	CaO , $\text{Ca}(\text{OH})_2$	Insoluble precipitate	Raises pH above 10

Evolution of Act. Sludge Process

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Chemical Addition Rates

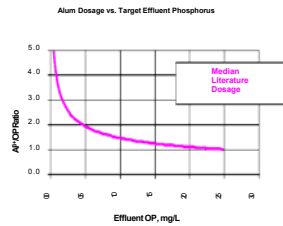
- Dependent on:
 - TP Discharge Limitations
 - Influx TP Loading
 - Biological P Removal Rates
 - Chemical to P Molar Ratios:
 - Al/Fe Salts, Range: 1.6- 2.1 to reach 0.5 mg/l P
 - > 3.0 to reach < 0.25 mg/l P
 - > 5.0 to reach < 0.2 mg/l P
 - >10 to reach < 0.15 mg/l P
 - Dependent on Alkalinity

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Phosphorus Removal w/Chemicals

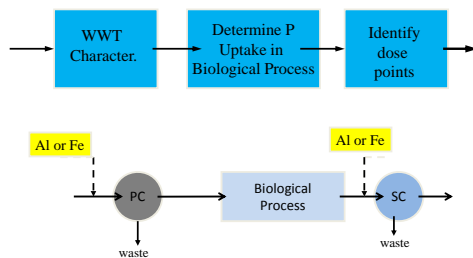
- Add chemical to precipitate phosphorus
- Alum & ferric chloride
- Consumes alkalinity
- **Increases sludge production**



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Chemical Addition Only Phosphorus Removal



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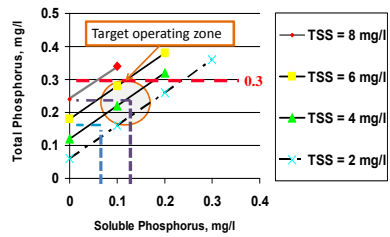
Gravity Filtration Application

- Removes Residual Bio-Floc
- Removes Residual Chemical/Bio Floc
- Removes Residual Coagulation Particles in Phys-Chem Treatment

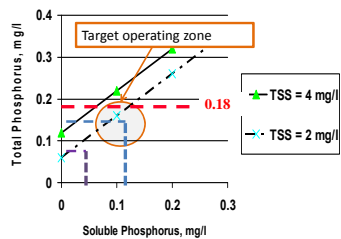
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Effluent TP versus Effluent TSS



Effluent TP versus Effluent TSS



Summary

Helpful Hints - Final Comments

Helpful Hints

- Consider multiple “barriers” for BOD, TN, and TP removal
- Nitrification is “Key” to successful nitrogen removal
- Nitrify completely – $\text{NH}_3 < 0.1 \text{ mg/l}$; no NO_2^-
- Maintain $< 0.1 \text{ mg/l}$ D.O. in denitrification process to maximize denitrification rate

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Final Comments

- Many possible causes for poor BOD and nutrient removal performance
- Important to determine cause and act quickly to maintain biological processes
- Basic troubleshooting approaches are universal
- Each plant should develop troubleshooting protocols that are specific to their specific processes, environmental conditions, and process control tools

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Questions?



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Thank You

"Anyone who can solve the problems of water will be worthy of two Nobel prizes – one for peace and one for science."

- John F. Kennedy



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The End



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